

# Introduction to Nastran SOL 200 Design Sensitivity and Optimization

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PRESENTED BY: CHRISTIAN APARICIO

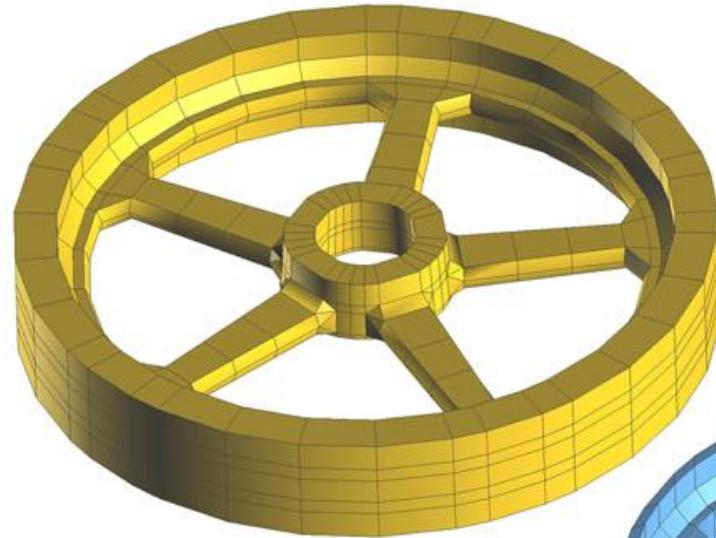
# Motivation

It is my intent that after you read this guide, you will be one step closer towards performing a unique procedure only a limited number of engineers can do.

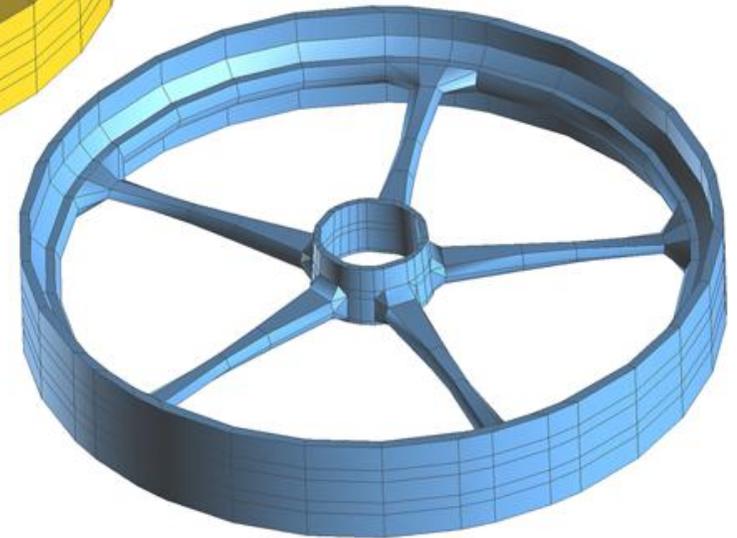
That is, optimizing structures automatically with Nastran SOL 200.

Kind Regards,

Christian Aparicio



BEFORE



AFTER

Shape Optimization is used to find optimum boundaries of this pulley

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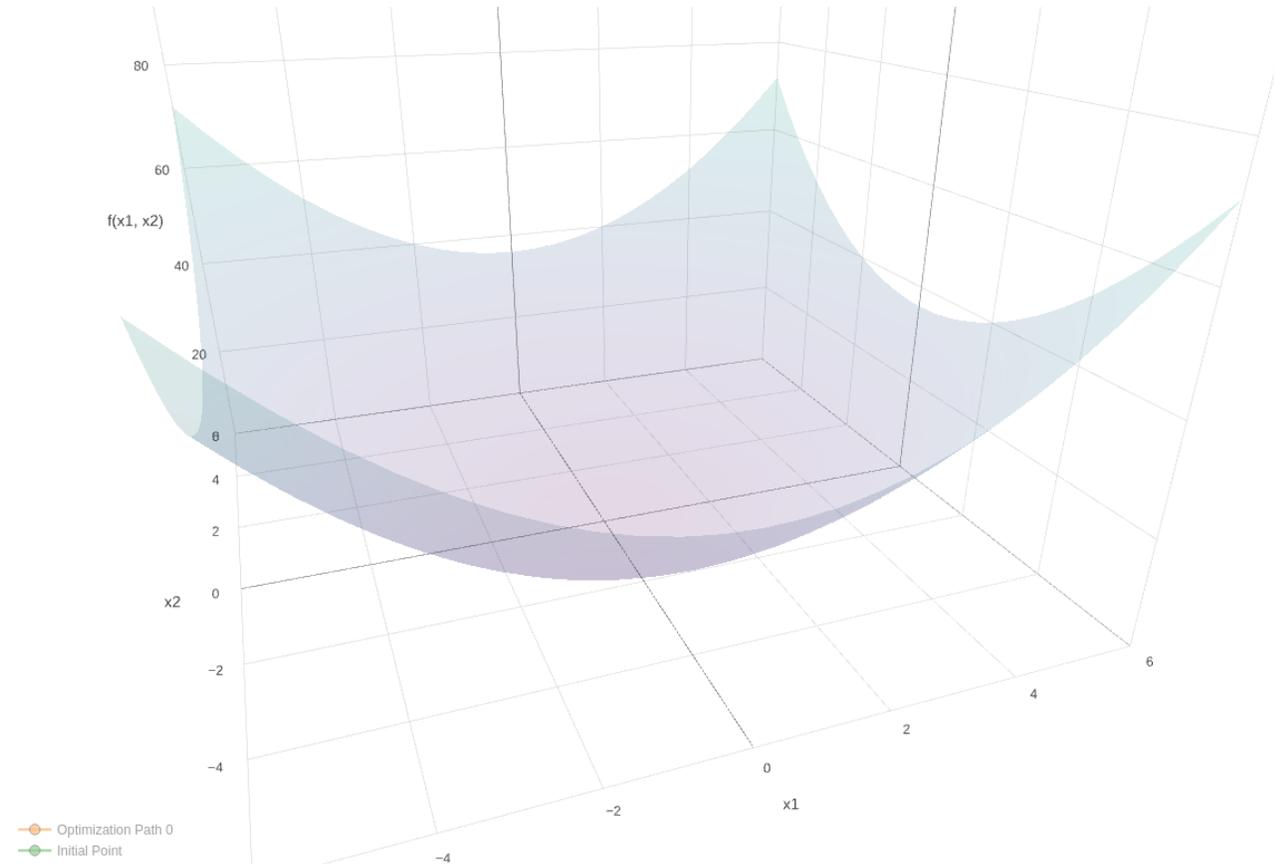
# What is optimization?

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$$f(x_1, x_2) = x_1^2 + x_2^2$$

Suppose we define and plot the function below:

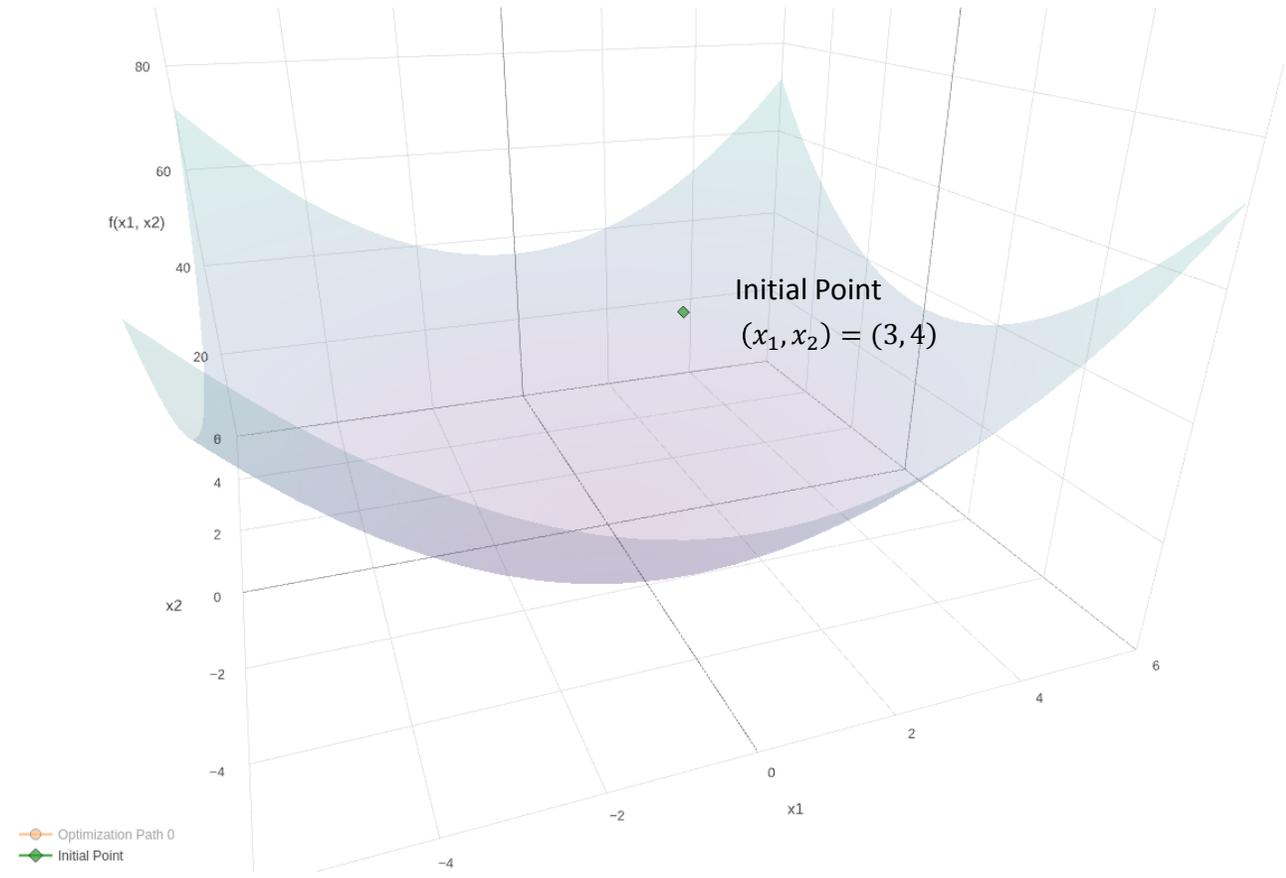
$$f(x_1, x_2) = x_1^2 + x_2^2$$



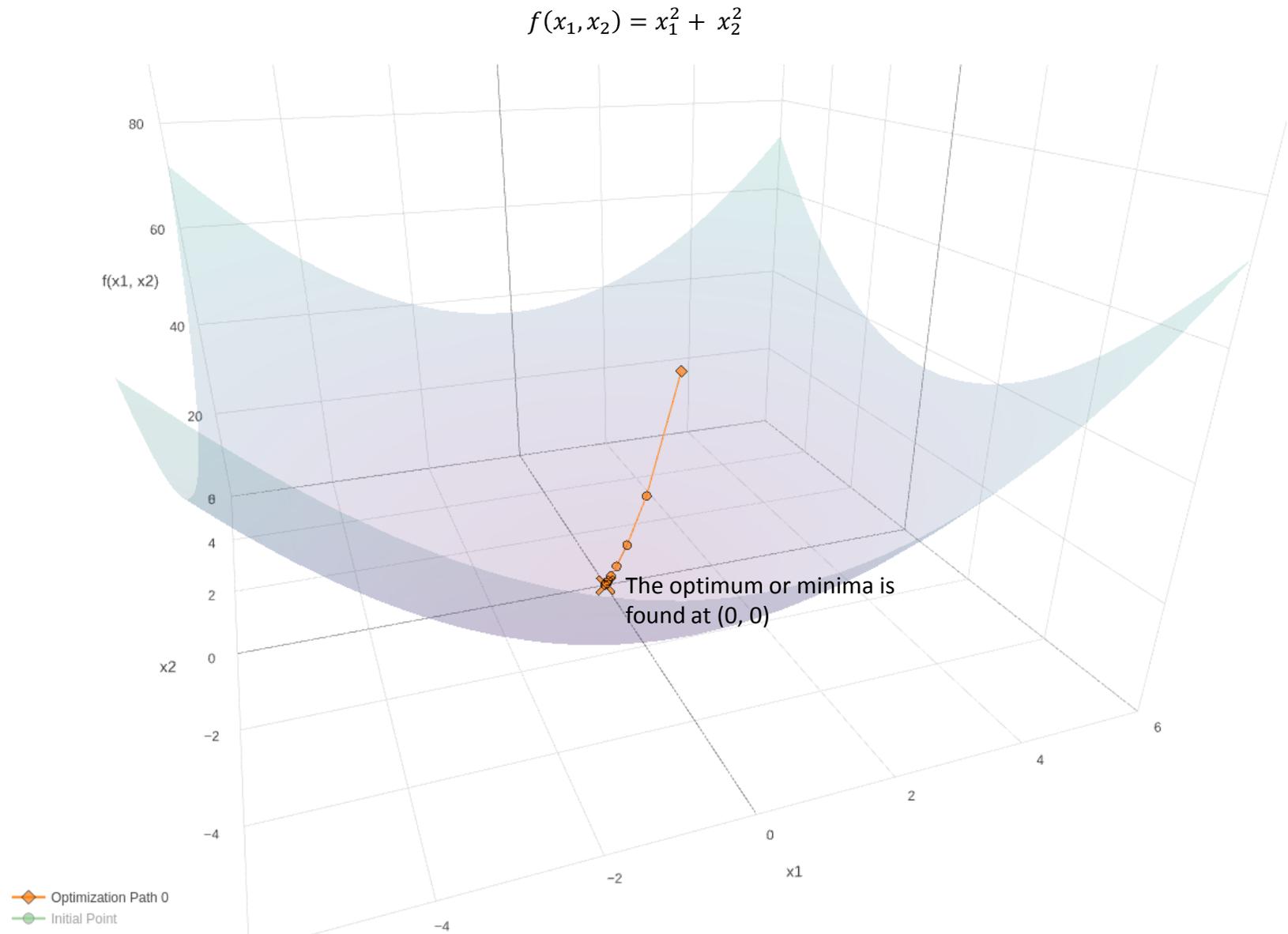
$$f(x_1, x_2) = x_1^2 + x_2^2$$

We start at point:  $(x_1, x_2) = (3, 4)$

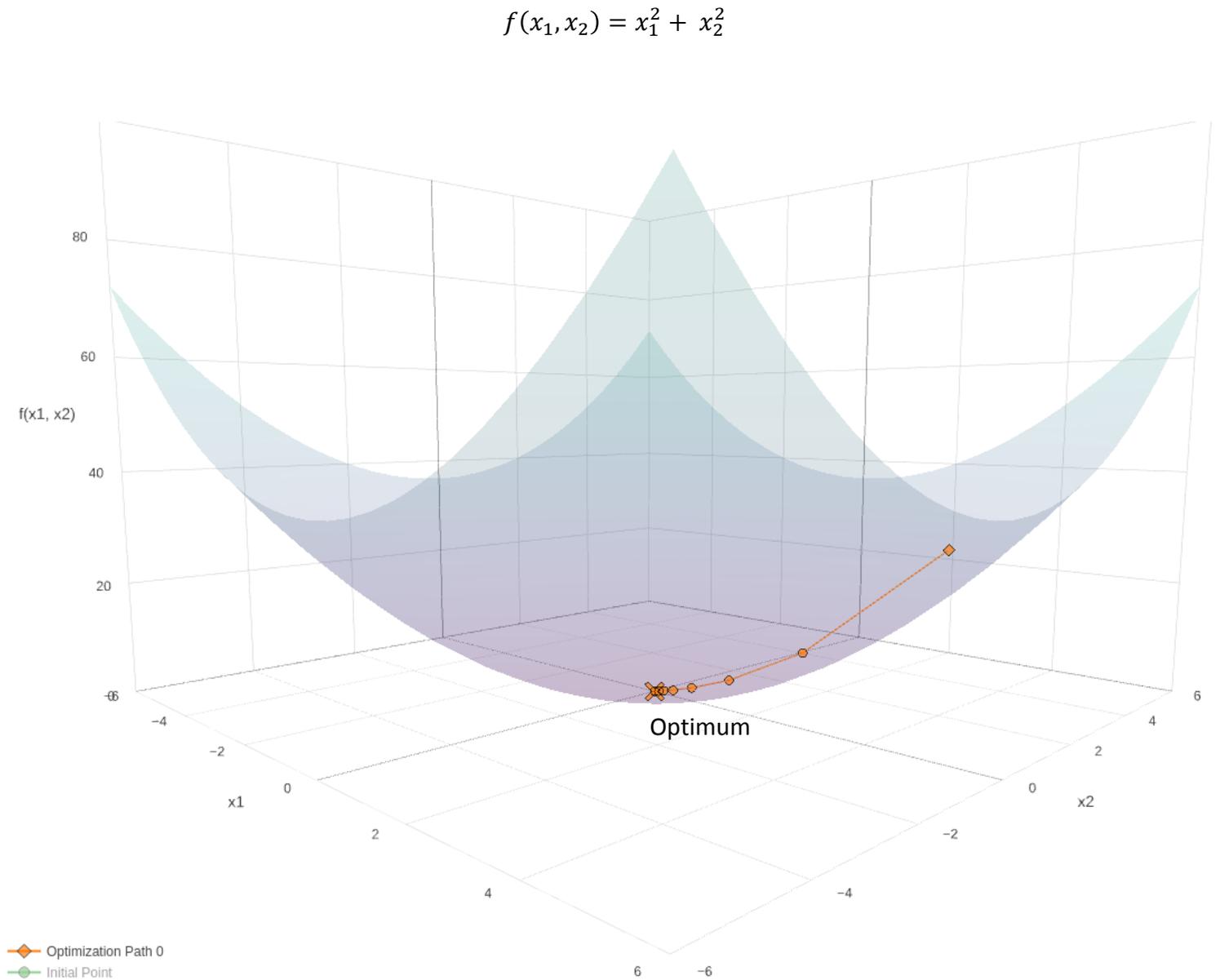
The objective is to find the minima of  $f(x_1, x_2)$



The optimizer in Nastran SOL 200 finds the minima at (0, 0).

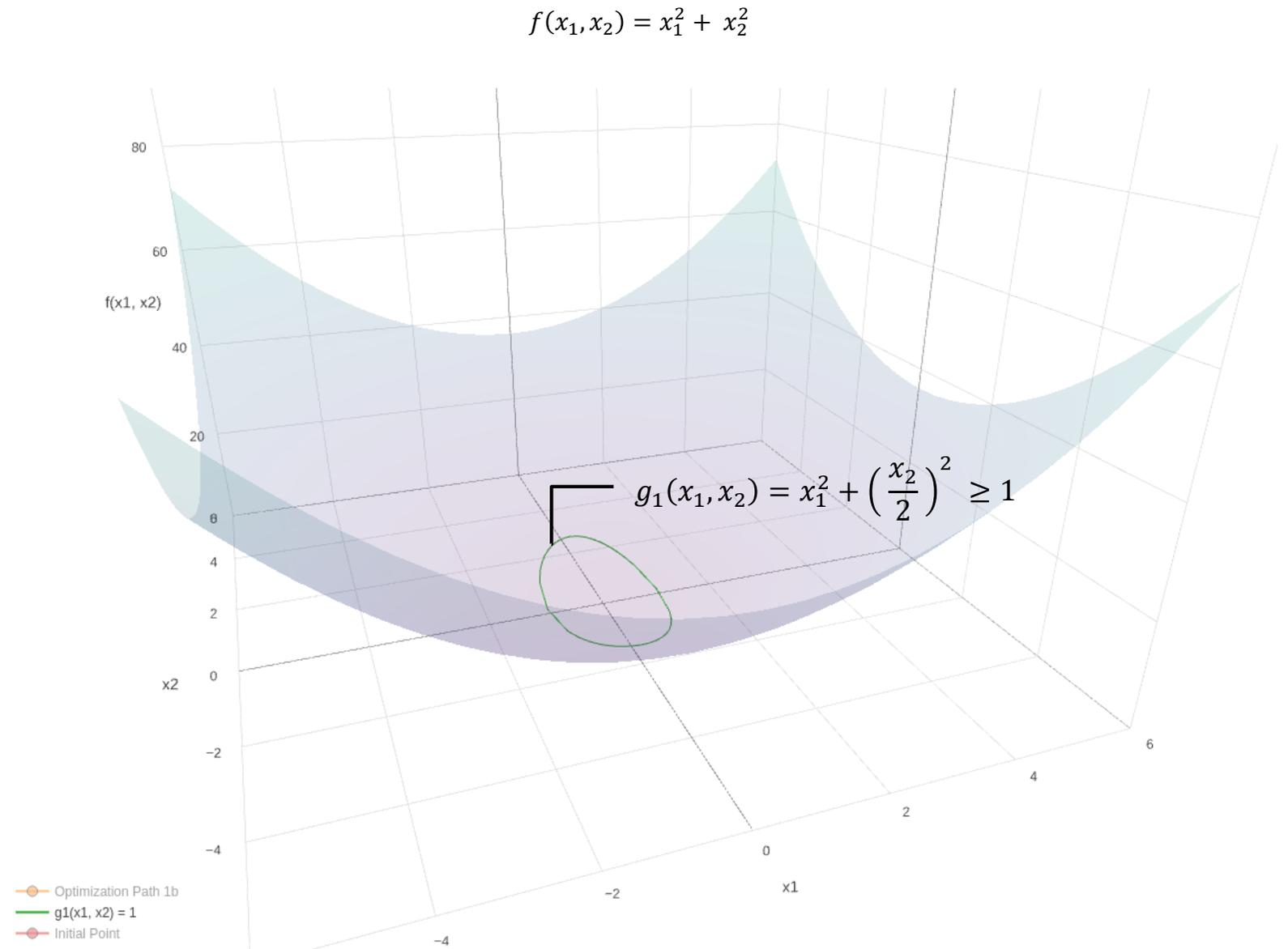


Optimization is the process of finding minima or maxima of functions.

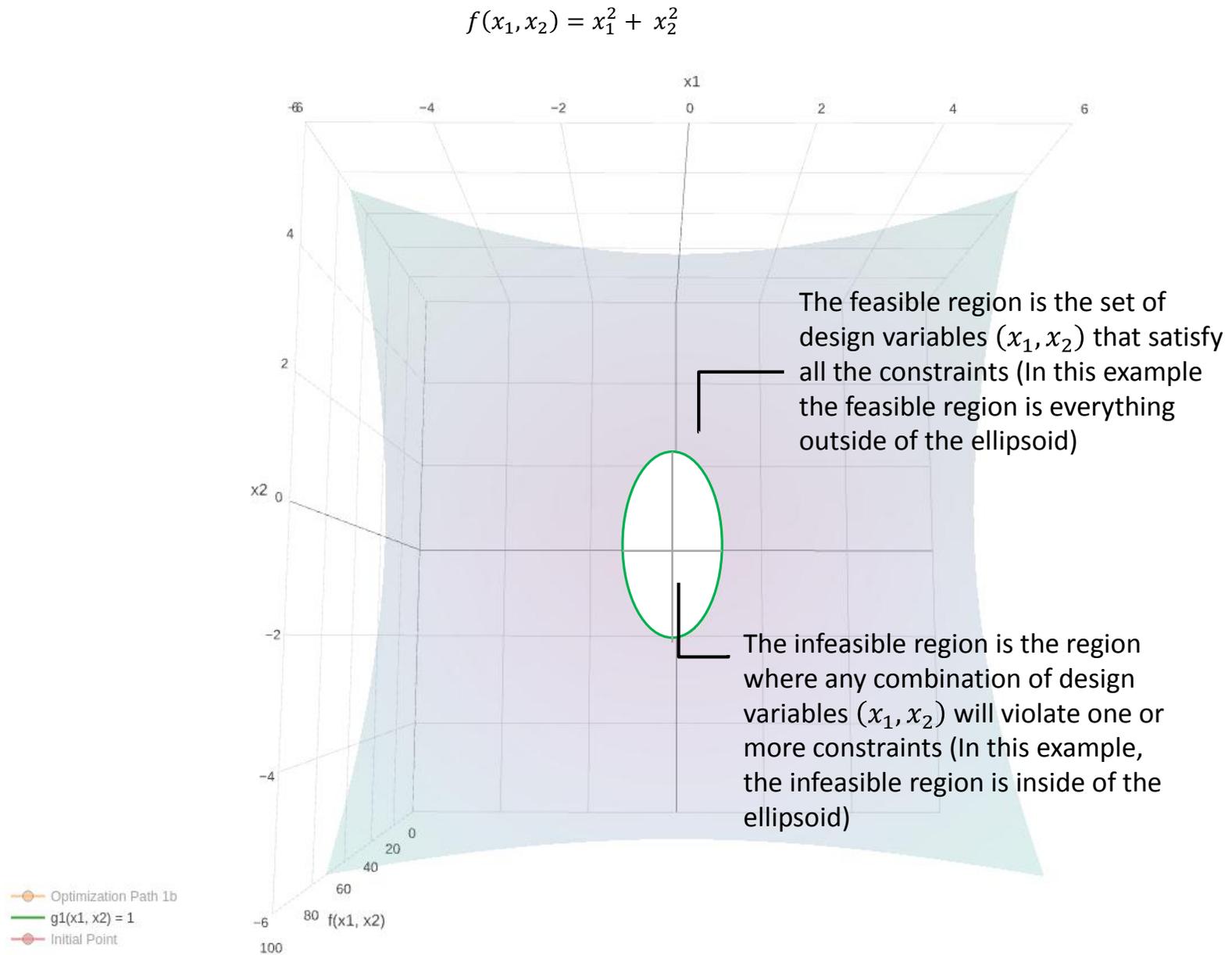


Let's continue the previous example and add this constraint:

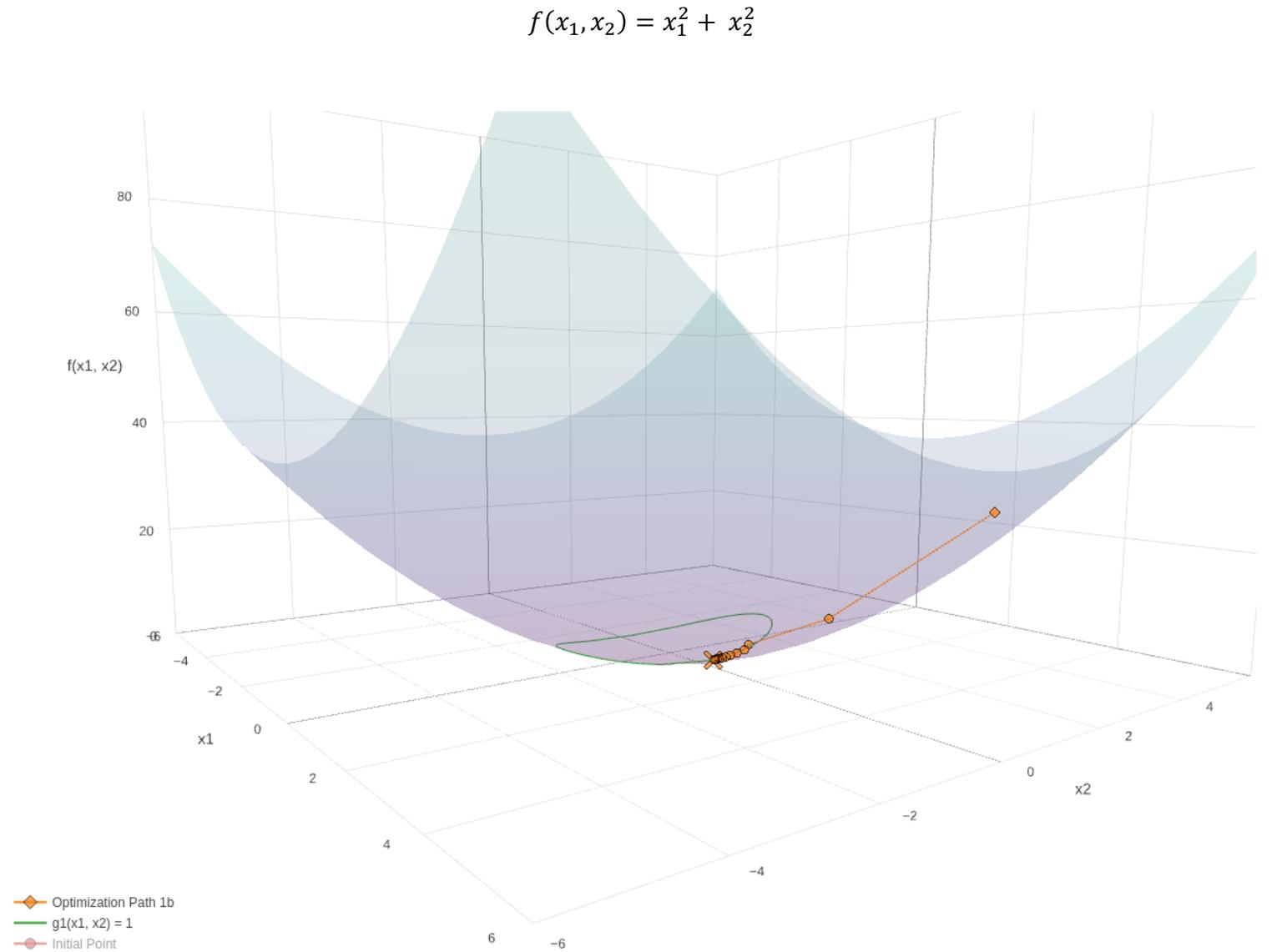
$$g_1(x_1, x_2) = x_1^2 + \left(\frac{x_2}{2}\right)^2 \geq 1$$



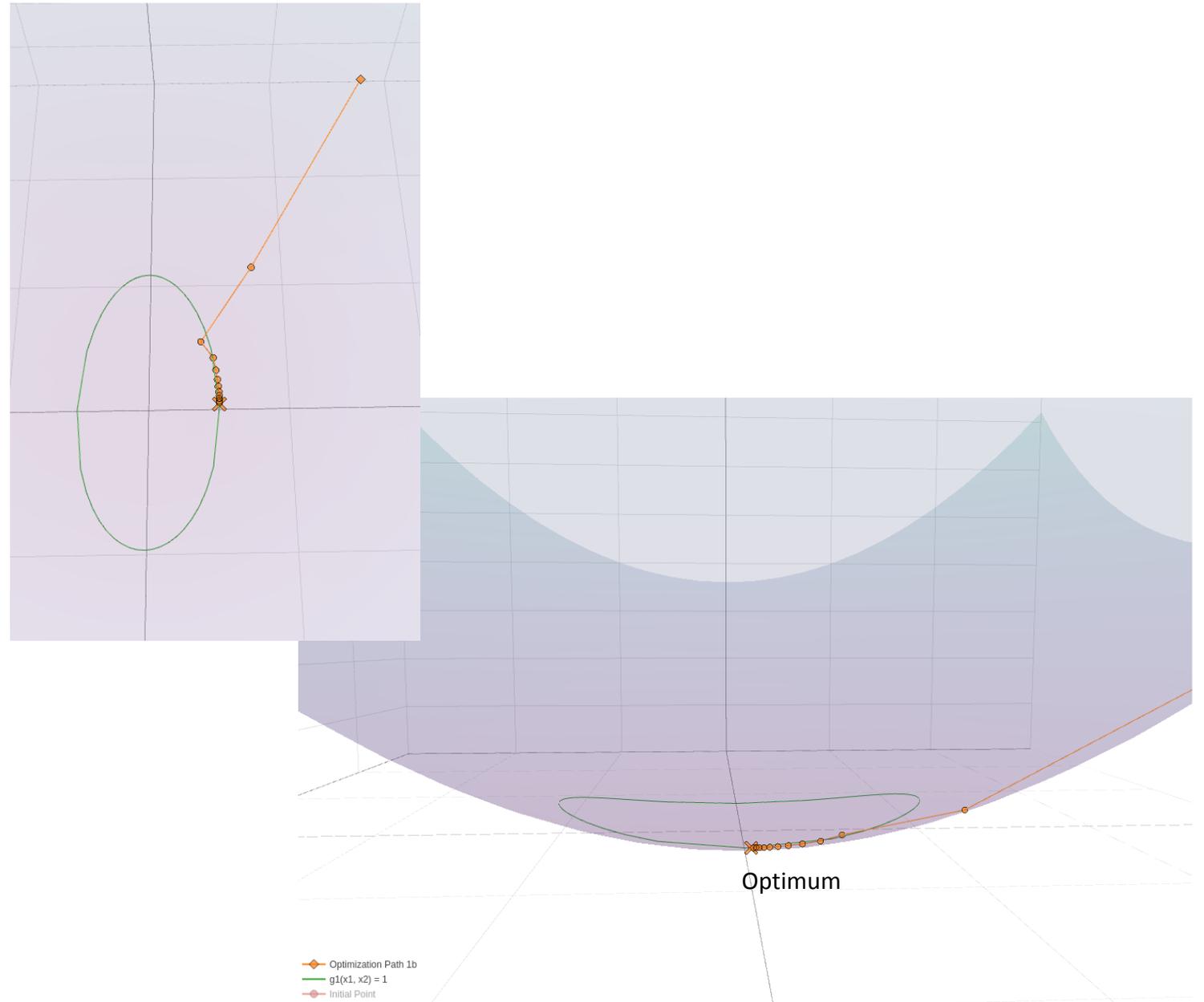
What does the optimizer do in this scenario? See next slide.



The optimizer will move towards the global minima



Once it reaches the constraint, the optimizer will move along the constraint until the minima is found



# What is the optimization problem statement?

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The optimization problem statement is composed of 3 items:

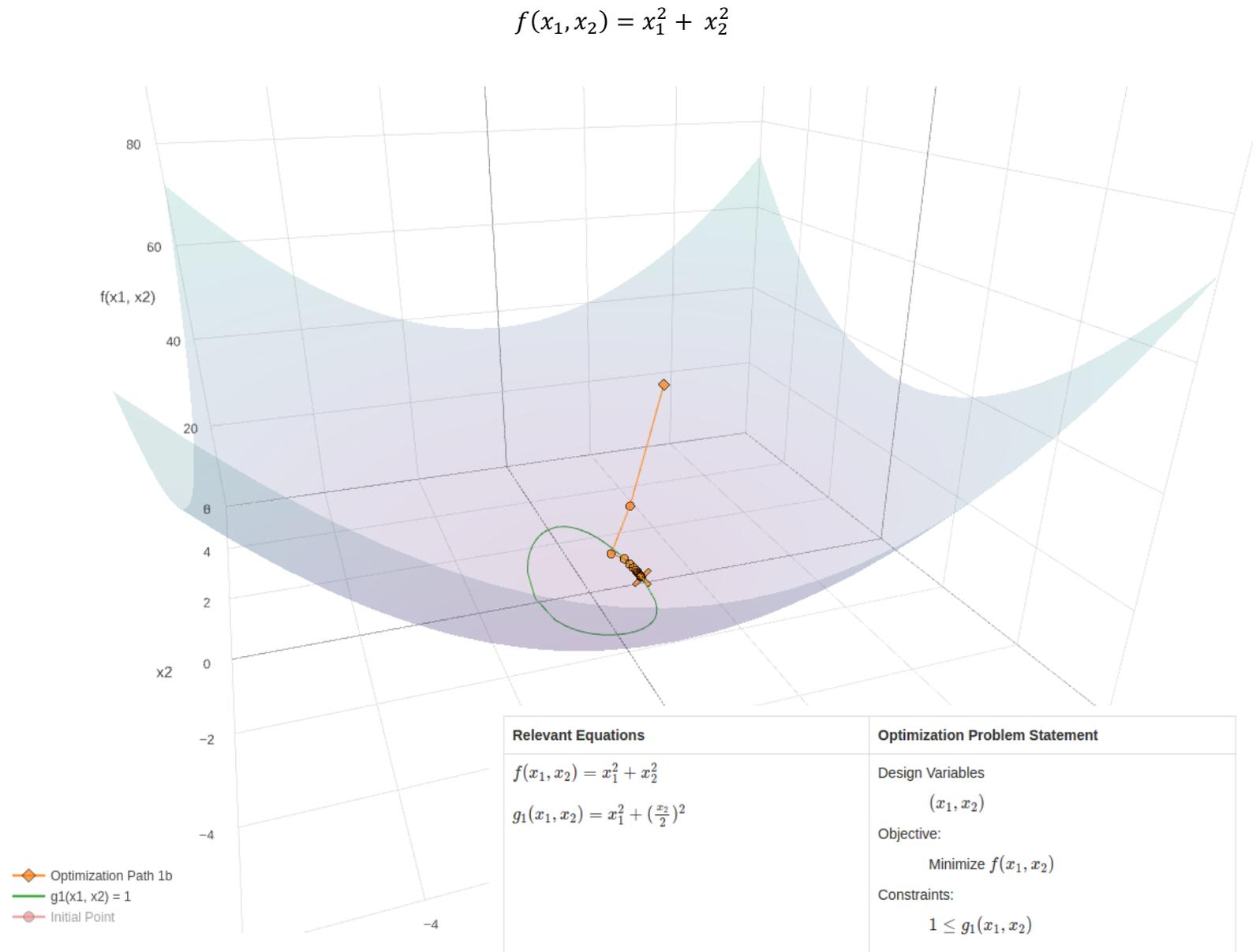
1. Design Variables – What parameters are allowed to vary?
2. Design Objective – What quantity is to be minimized or maximized?
3. Design Constraints – What quantities are constrained?

This is the optimization problem statement for the last example



Relevant Equations	Optimization Problem Statement
$f(x_1, x_2) = x_1^2 + x_2^2$ $g_1(x_1, x_2) = x_1^2 + \left(\frac{x_2}{2}\right)^2$	Design Variables $(x_1, x_2)$ Objective: Minimize $f(x_1, x_2)$ Constraints: $1 \leq g_1(x_1, x_2)$

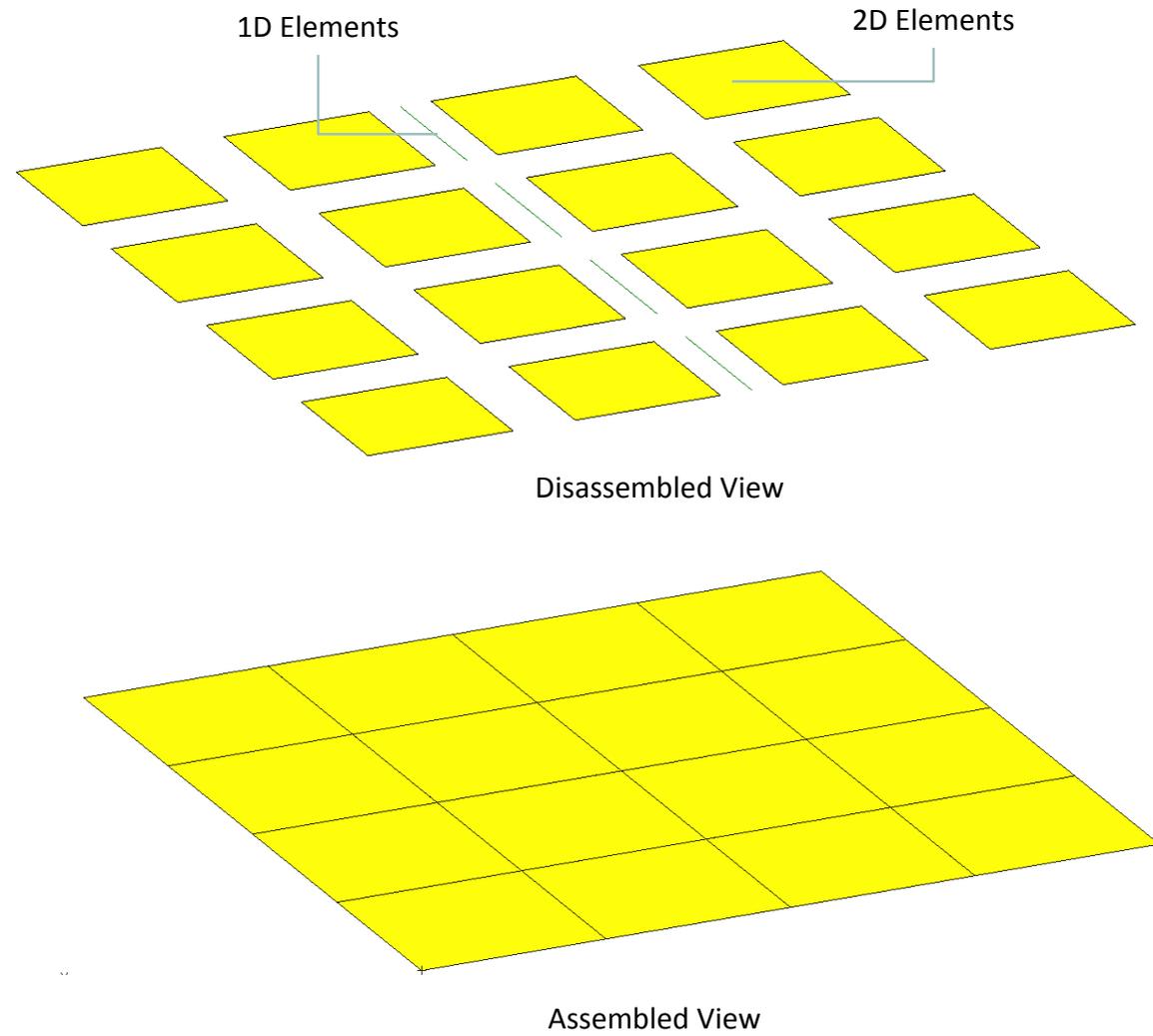
It is important to always have the optimization problem statement drafted before performing an optimization



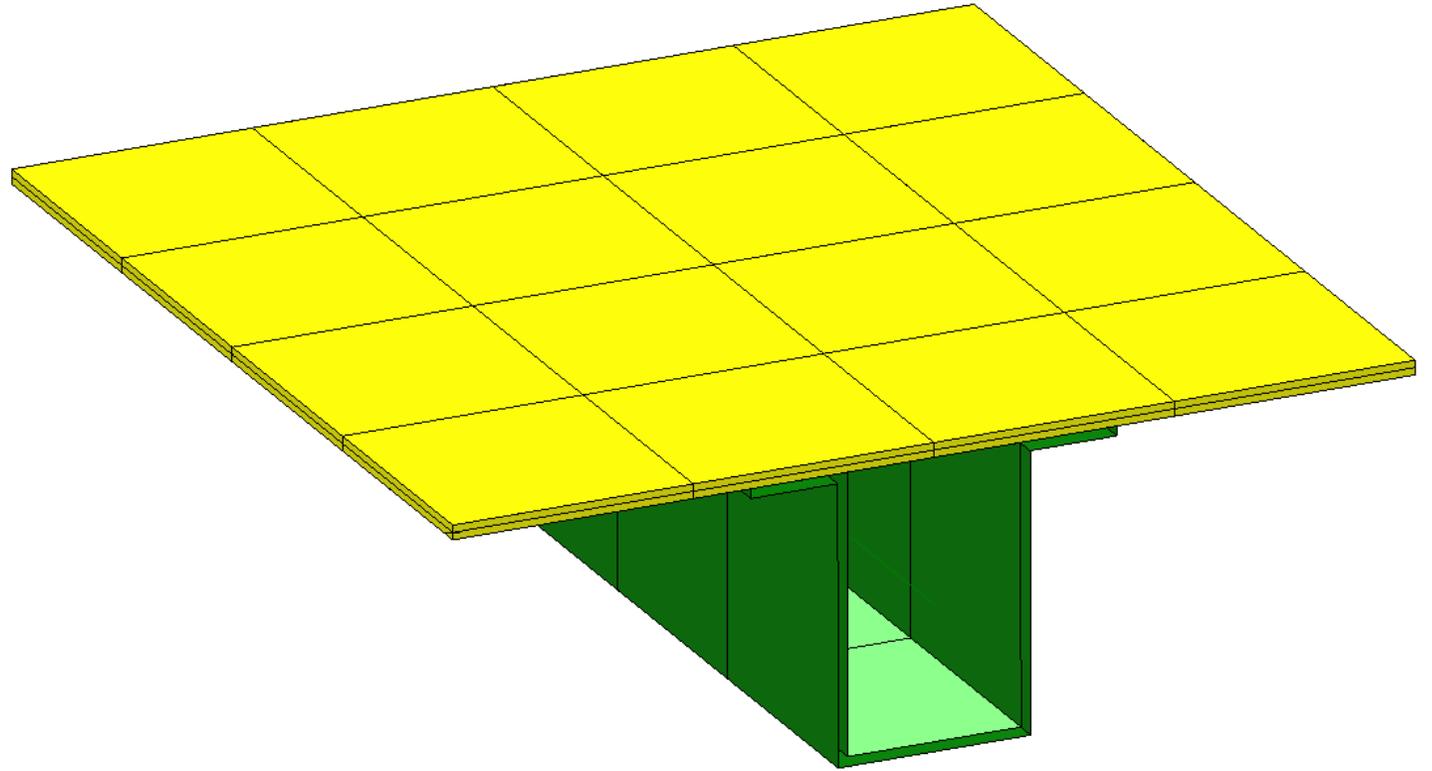
# What is size optimization?

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Consider the example finite element model to the right.



After assigning parameters such as thickness to the 2D elements and beam cross section dimensions to the 1D elements, the structure looks as shown on the right.

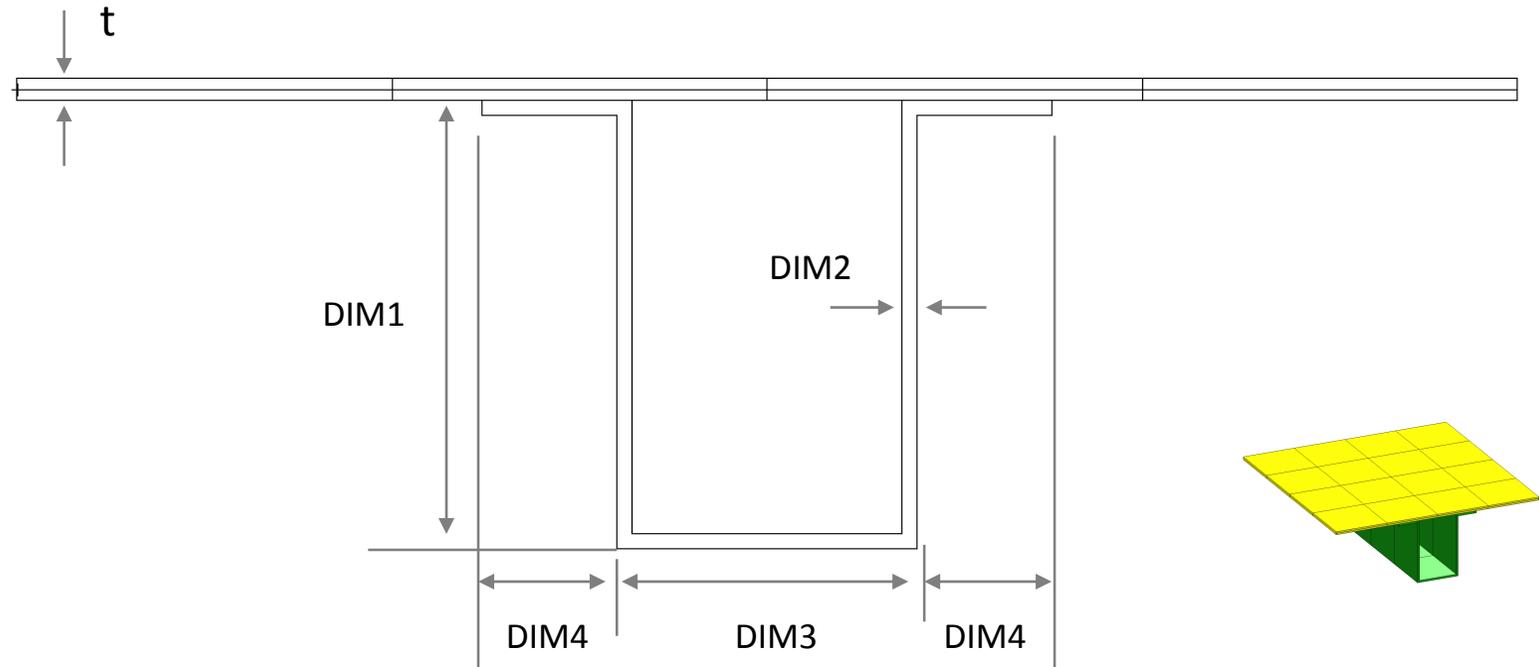


Size optimization is the process of setting parameters as design variables.

For example, the thickness and dimension 1 and 2 can be set as design variables.

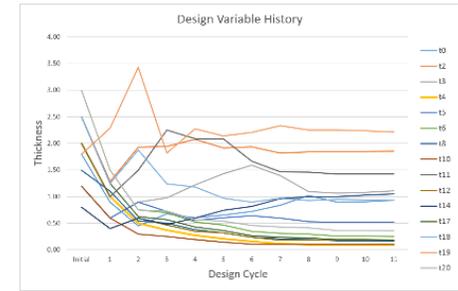
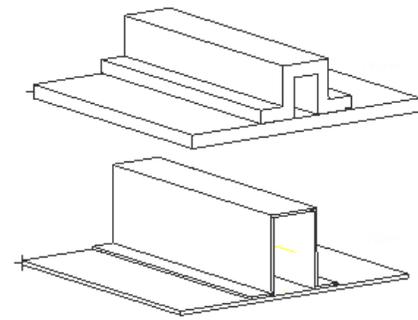
- $x_1$ :  $t$ , thickness
- $x_2$ : DIM1
- $x_3$ : DIM2

Other parameters that can be set as design variables include: Young's modulus or density of a material. The complete list of parameters that can be set as design variables is extensive.

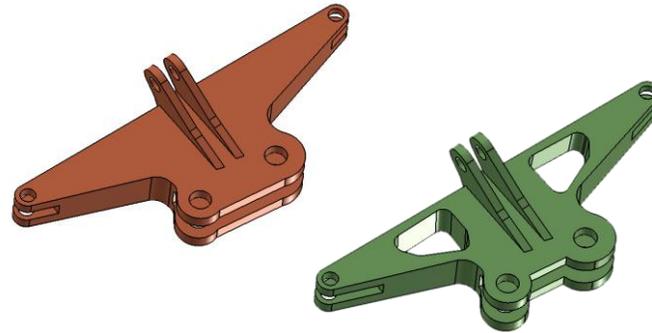


Note that many optimization types exist. To the right are some of the many types.

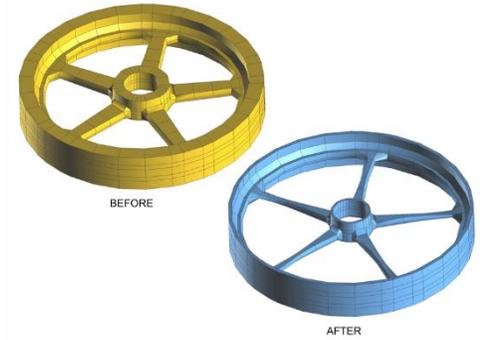
The remainder of this guide will only apply to size optimization.



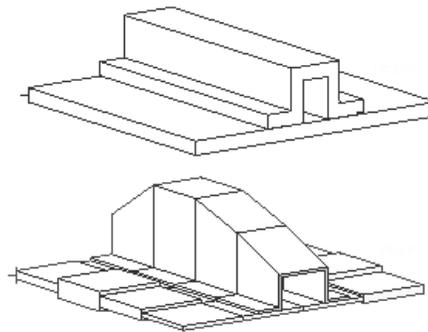
Size Optimization



Topology Optimization



Shape Optimization



Topometry Optimization



Topography Optimization

# Optimization Examples with Nastran SOL 200

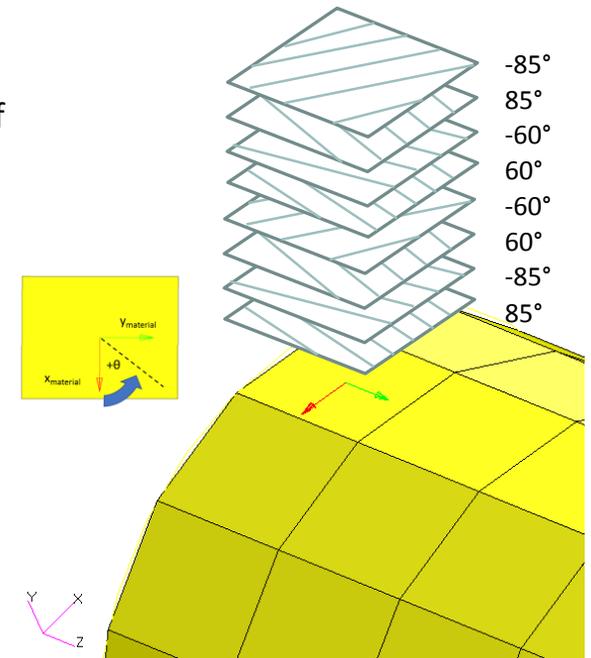
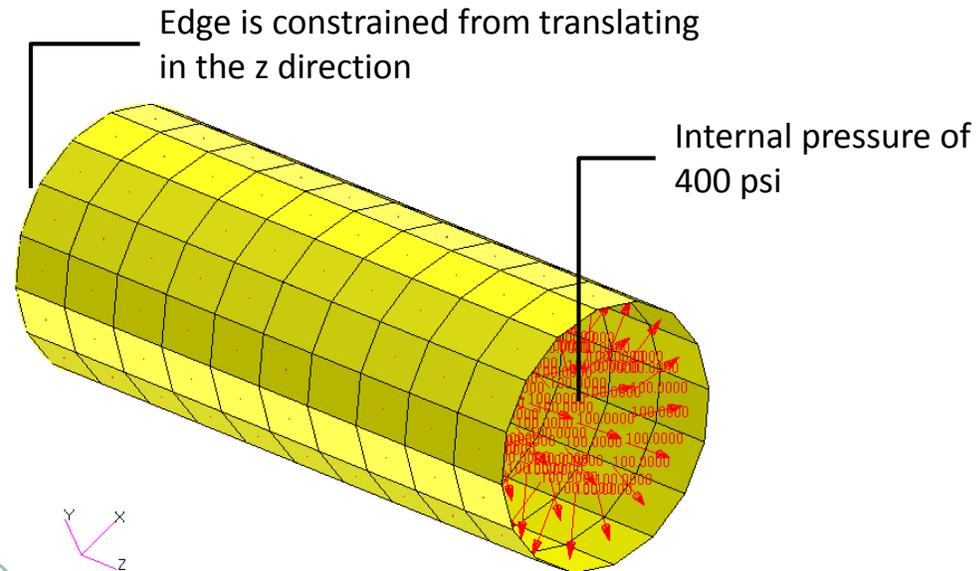
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# Example 1 - Optimization of a composite laminate

A cylindrical tube is composed of a composite laminate with the following layup: [85/-85/60/-60/60/-60/85/-85]. Each ply has a thickness of .01 inches.

## Loading and Constraints

The tube is allowed to freely expand radially outward. An internal pressure of 400 psi is applied.



[Click here to watch this tutorial](#) 

# Example 1 - Optimization of a composite laminate

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## Optimization Problem Statement

- Design Variables:
  - Thickness Variables
    - x1, x2, x3, x4, x5, x6, x7, x8 correspond to the thickness of lamina 1 through 8, respectively
    - Each thickness variable shall be equal to x1
    - x1 is allowed to range between .001 and 10.
  - Orientation Variables
    - x9, x10, x15, x16 correspond to the outer layer pair angles, i.e. 85 degree plies
    - x11, x12, x13, x14 correspond to the core pair angles, i.e. 45 degree plies
    - The orientation angles are allowed to vary between -90. and 90 degrees
- Laminas 1, 2, 7, 8 should have the same orientation angle, but with opposing signs
- Laminas 3, 4, 5, 6 should have the same orientation angle, but with opposing signs
- The orientation angles are only allowed to be in 5 degree increments, e.g. 90, 85, 80... -80, -85, -90

### Design Objective

- Minimize the weight

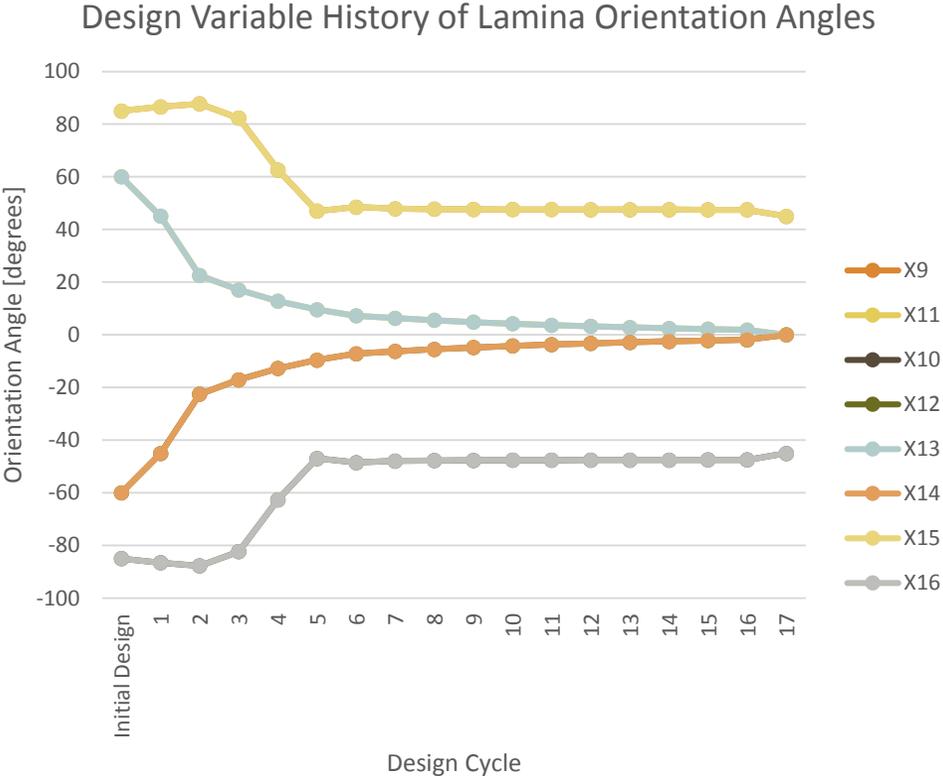
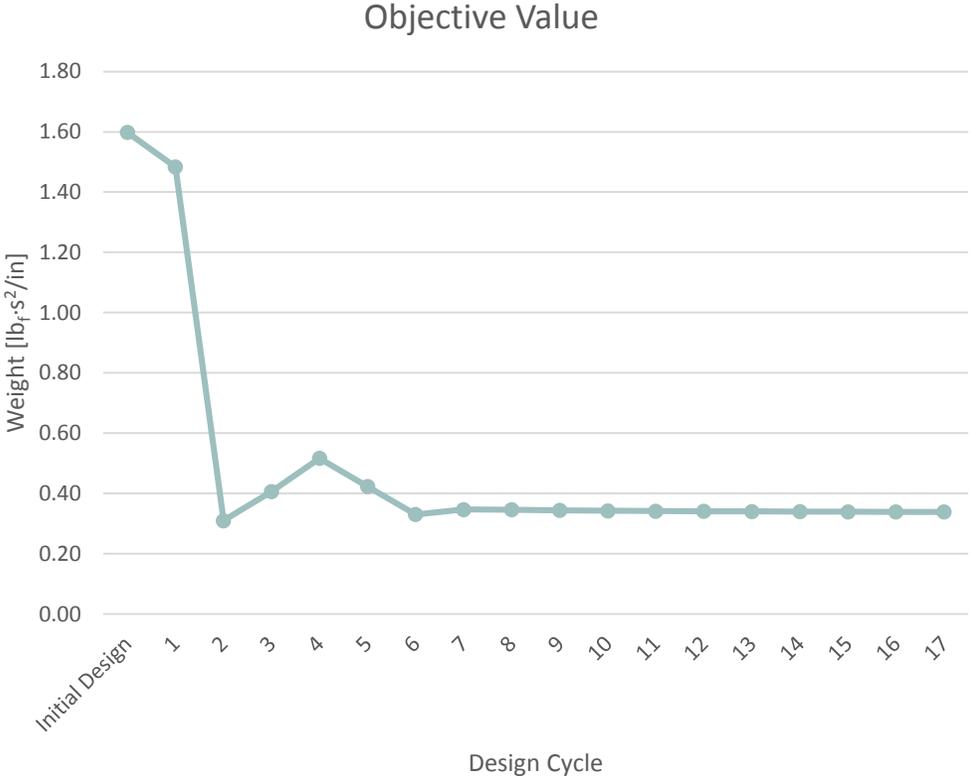
### Design Constraints

- The strength ratio for each lamina shall be less than .9

## Optimization Results

- Initial Design
  - Mass: 1.60 lb<sub>f</sub>·s<sup>2</sup>/in
  - Layup: [85/-85/60/-60/60/-60/85/-85]
  - Ply Thicknesses: .0100 in.
  - Max strength ratio: 21.0
- Optimized Design
  - Mass: .3386 lb<sub>f</sub>·s<sup>2</sup>/in
  - Layup: [45/-45/0/0/0/0/45/-45]
  - Ply Thicknesses: .0021 in.
  - Max strength ratio: .9

# Example 1 - Optimization of a composite laminate



# Example 2 - Model Matching / System Identification / Correlation to Experiment

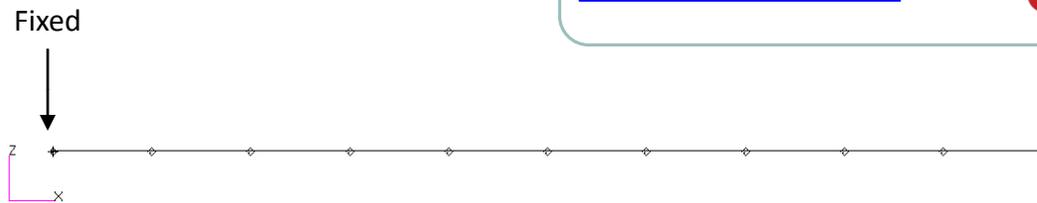
A beam, fixed on one end, has a circular cross section with a radius of 2 in. The length of the beam is 30 in. Experiment has revealed the expected mode shapes for modes 1 and 3. A modes analysis of the finite element (FE) models shows a discrepancy between the FE model and experiment.

Optimization is used to find a radius of the cross section that will produce FE results comparable to experiment.

## Experimental Results

Mode 1			Mode 3	
Node	Component	Value	Component	Value
3	z or 3 direction	0.0143	x or 1 direction	0.1204
6	z or 3 direction	0.1741	x or 1 direction	0.5431
9	z or 3 direction	0.6381	x or 1 direction	0.9216

[Click here to watch this tutorial](#) 



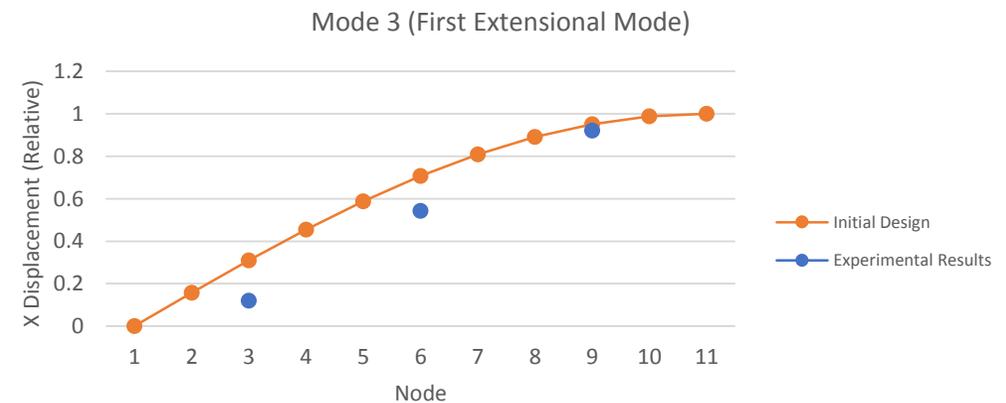
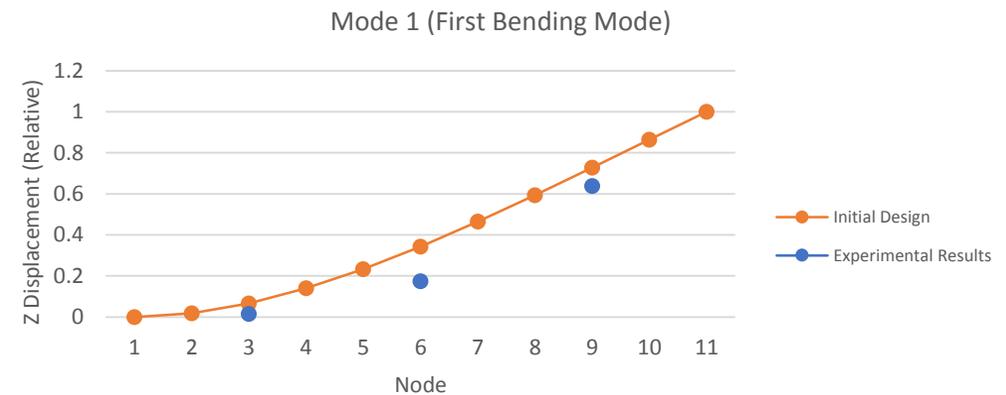
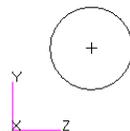
Length: 30 in

$E = 1 * 10^7$  psi

$\nu = .3$

Density =  $.01 \text{ lb}_f * \text{s}^2 / \text{in}^4$

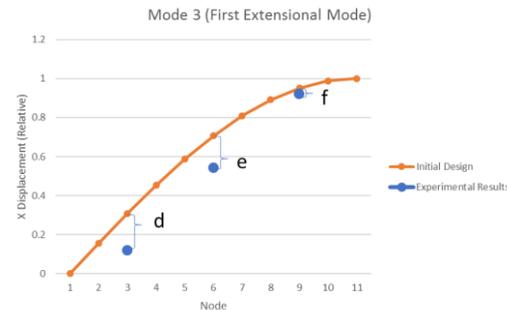
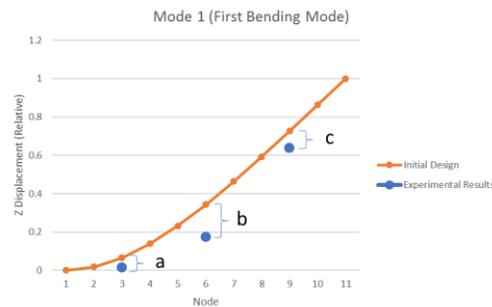
Radius: 2in



# Example 2 - Model Matching / System Identification / Correlation to Experiment

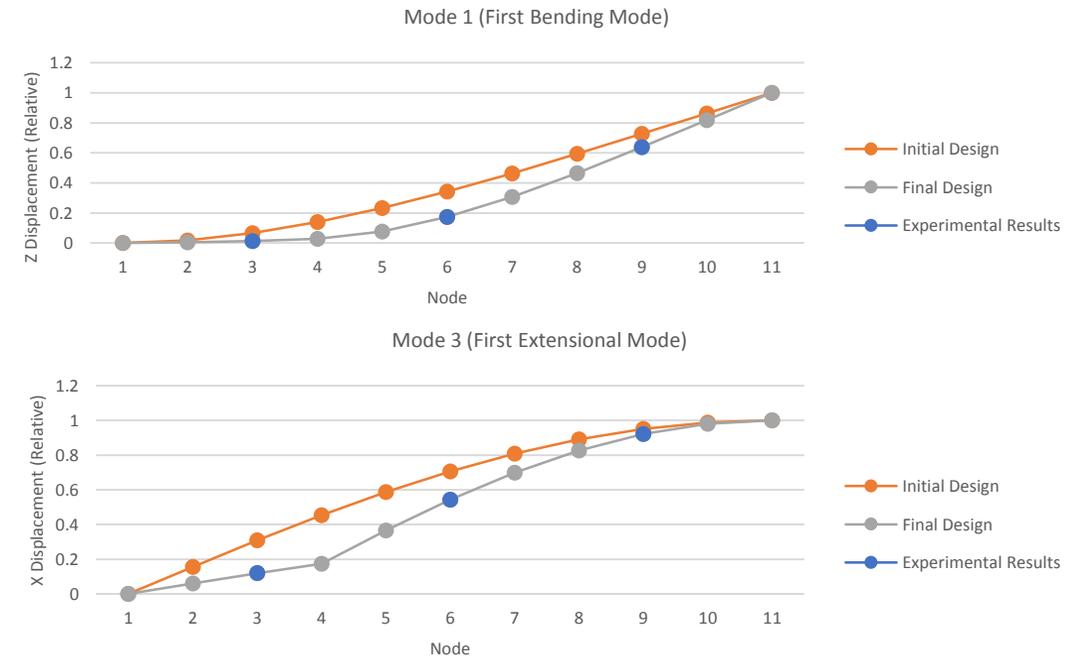
## Optimization Problem Statement

- Design Variables:
  - x1: The radius of 3 elements is allowed to vary between .1 and 10. inches.
- Design Objective
  - Experimental data is available regarding the 1<sup>st</sup> mode shape
  - The objective is to minimize the root sum of squares (RSS) between the experiment and FE results
    - $f = \text{RSS} = \sqrt{a^2 + b^2 + c^2}$ 
      - a = (.0143 - r801)
      - b = (.1741 - r802)
      - c = (.6381 - r803)
      - r801, r802, r803 are the z displacements at nodes 3, 6, 9, respectively, for mode 1
- Design Constraint
  - The RSS of mode 3 is to be less than .002
    - $g1 = \text{RSS} = \sqrt{d^2 + e^2 + f^2}$ 
      - d = (.1204 - r501)
      - e = (.5431 - r502)
      - f = (.9216 - r503)
      - r501, r502, r503 are the x displacements at nodes 3, 6, 9, respectively, for mode 3

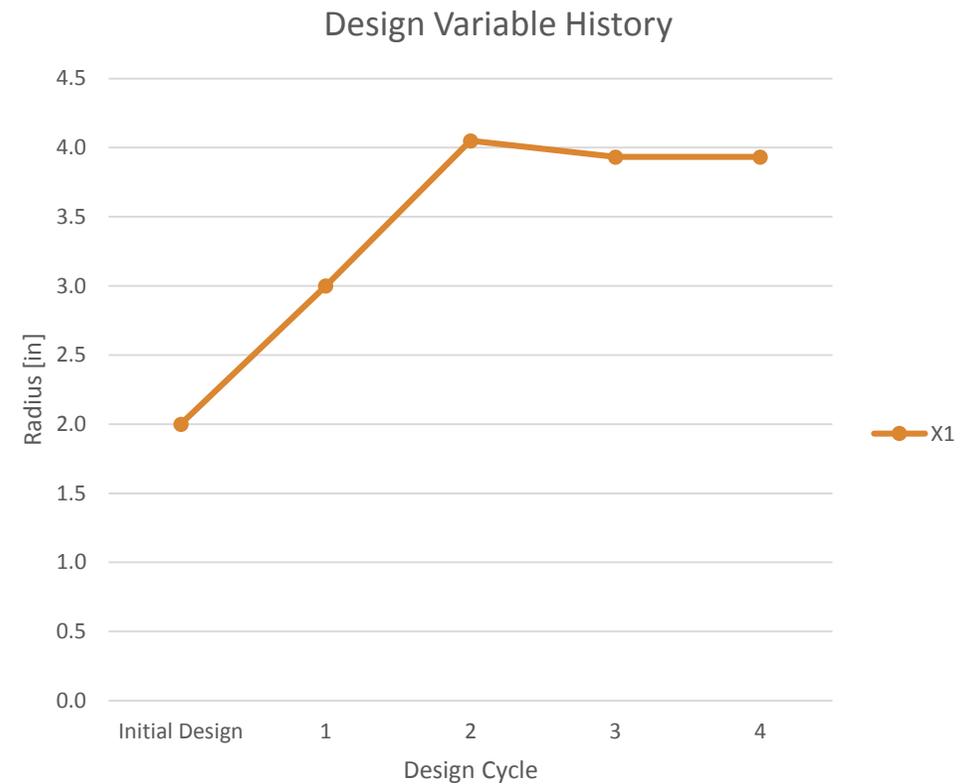
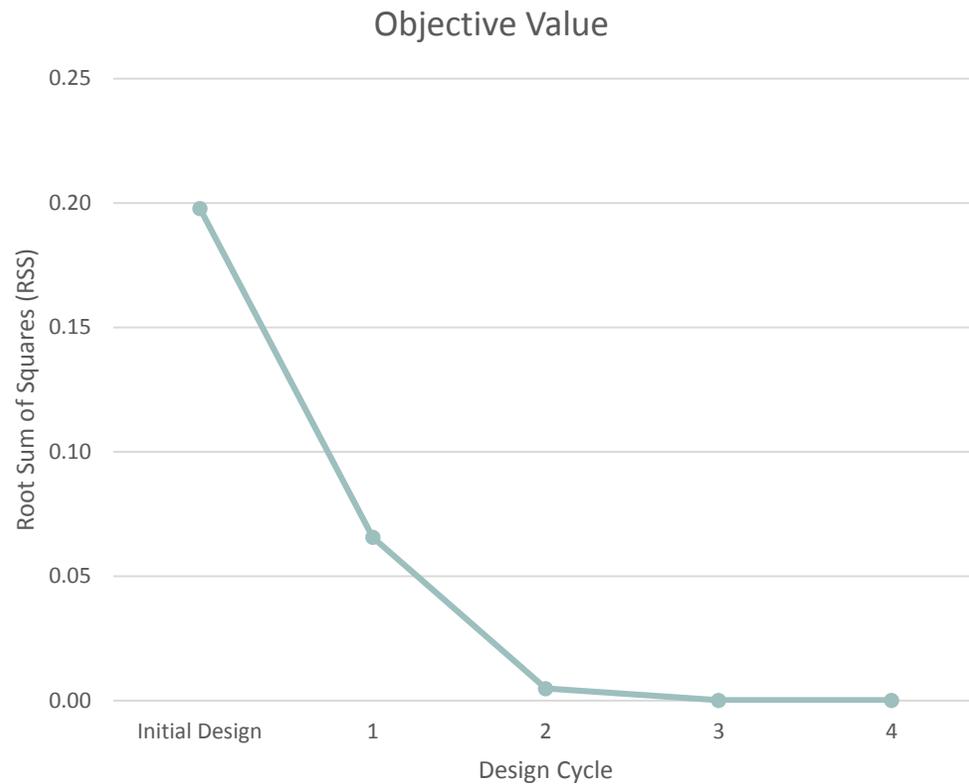


## Optimization Results

- The following plots show the values for the mode shapes of the initial design and optimized design. Note that the optimized or final design has normal mode shapes that align with experiment



# Example 2 - Model Matching / System Identification / Correlation to Experiment

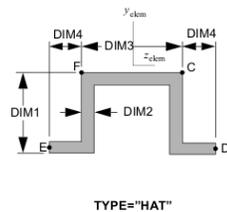


# Example 3 – Buckling Optimization of a Thin Walled Cylinder

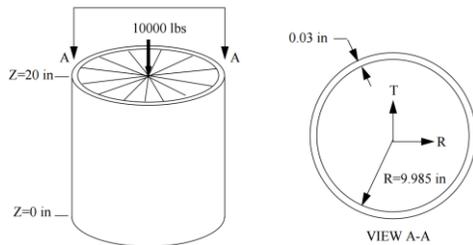
A thin walled cylinder reinforced with ring stiffeners is subjected to an axial compressive load. The initial design is far from exceeding the allowable stresses in the stiffeners and wall. The buckling factor is well above 1, so buckling will not occur.

Optimization is used to vary two structural dimension, wall and stiffener thickness, so as to

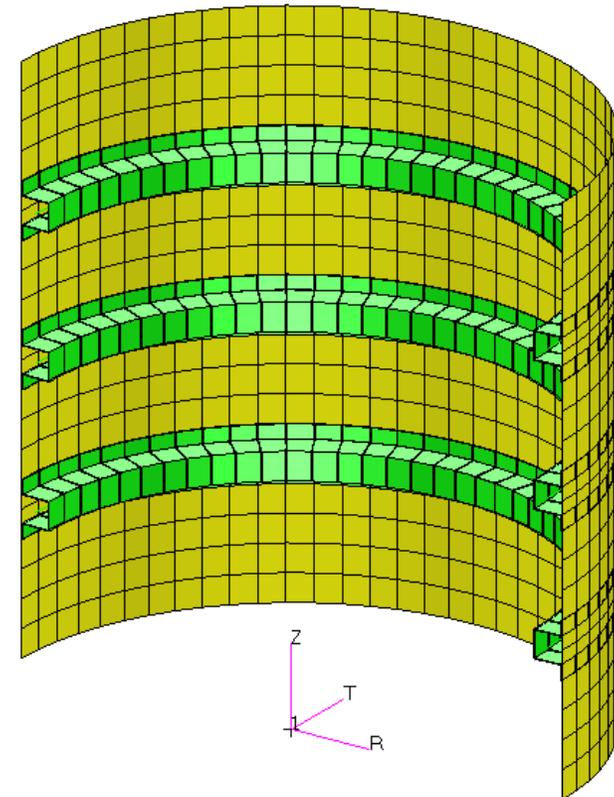
minimize the mass of the structure while ensuring stress is not exceeded and buckling does not occur. This optimization is an example of multi-discipline optimization since the structure is optimized for both static and buckling analyses.



- DIM1: 1 in.
- DIM2: .03 in
- DIM3: 1 in.
- DIM4: .5 in



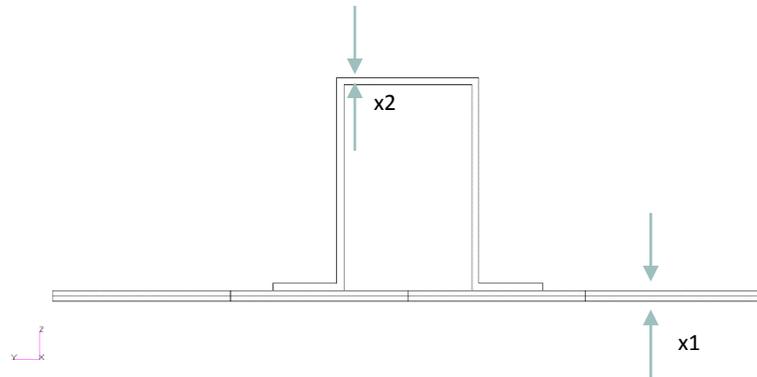
[Click here to watch this tutorial](#) 



# Example 3 – Buckling Optimization of a Thin Walled Cylinder

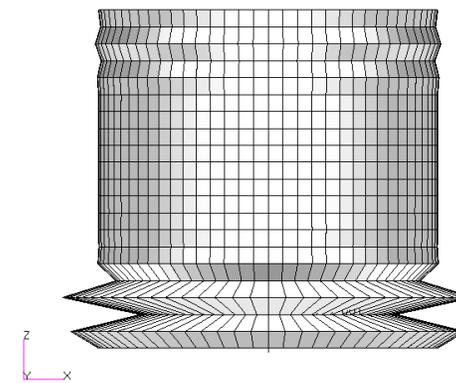
## Optimization Problem Statement

- Design Variables:
  - x1: The thickness of the thin wall is allowed to vary. Bounds:  $.001 < x1 < 10$ .
  - x2: The thickness of the stiffener cross section is allowed to vary. Bounds:  $.001 < x2 < 10$ .
- Design Objective
  - Minimize Weight
- Design Constraints
  - Statics Subcase
    - The maximum beam stress in the stiffener is allowed to be no greater than 25000.
    - The maximum von Mises stress for the z1 and z2 fibers of the thin wall shall be no greater than 25000.
  - Buckling Subcase
    - The buckling load factor shall be no less than 1.0

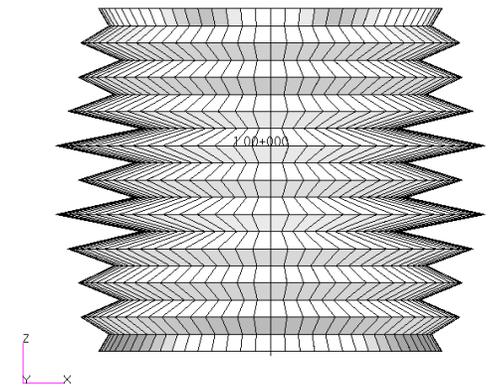


## Optimization Results

- Initial Design
  - Mass: 5.76 lbf
  - x1 = Thickness of wall = .03 in
  - x2 = Thickness of stiffener = .03 in
  - Buckling factor = 3.6
  - Stiffener and shell stresses within limits
- Optimized Design
  - Mass: 1.77 lbf
  - x1 = Thickness of wall = .0135 in
  - x2 = Thickness of stiffener = .0016 in
  - Buckling factor =  $.99 \approx 1.0$
  - Stiffener and shell stresses within limits

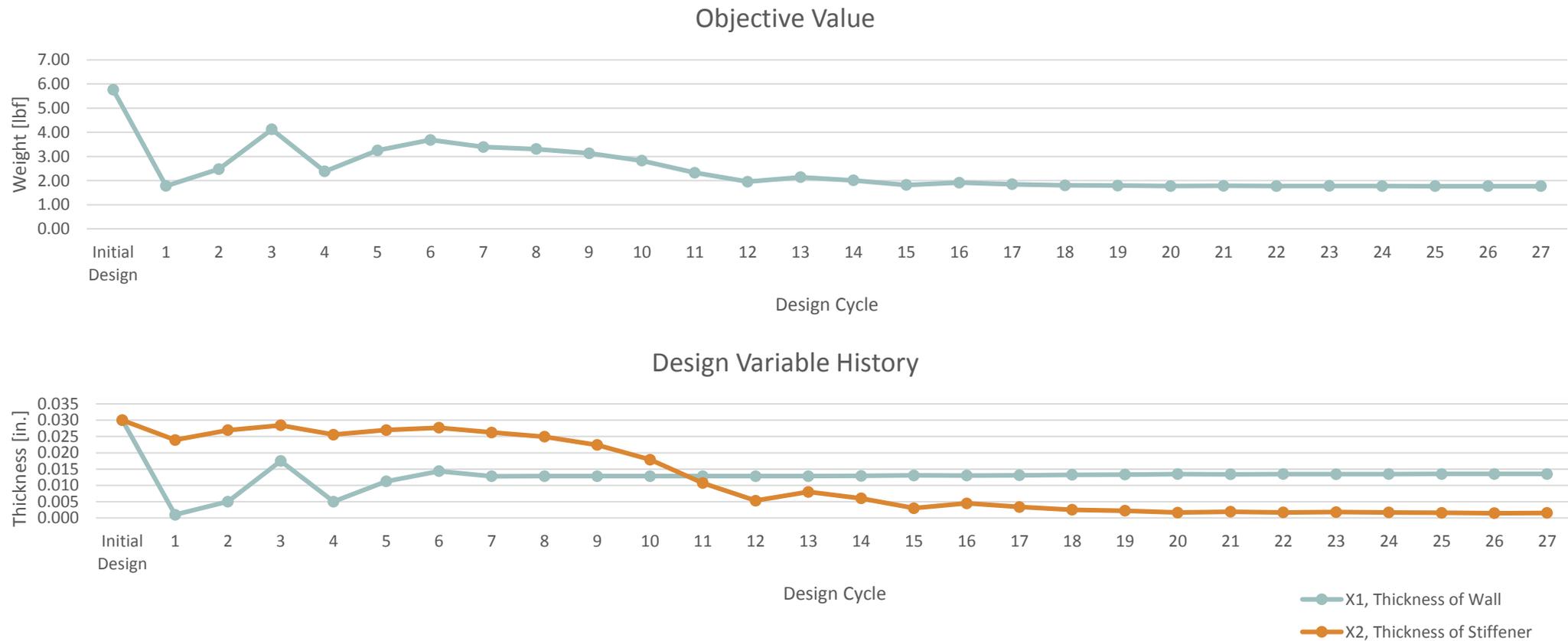


Buckling Shape (B.F. = 3.6)



Buckling Shape (B.F. = .99)

# Example 3 – Buckling Optimization of a Thin Walled Cylinder



# How to Set Up Nastran SOL 200

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A STEP-BY-STEP PROCEDURE FOR CONVERTING .BDF OR .DAT FILES  
TO SOL 200



## Three-Bar Truss Optimization Example

This example can be found in the MSC Nastran Design Sensitivity and Optimization User's Guide. The text and images below have been extracted from that user's guide.

"A common task in design optimization is to reduce the mass of a structure subjected to several load conditions. Figure 8-1 shows a simple three-bar truss that must be built to withstand two separate loading conditions. Note that these two loads subject the outer truss members to both compressive as well as tensile loads. Due to the loading symmetry, we expect the design to be symmetric as well. As an exercise, we'll show how to enforce this symmetry using design variable linking." - *MSC Nastran Design Sensitivity and Optimization User's Guide, Chapter 8: Example Problems, Three-Bar Truss*

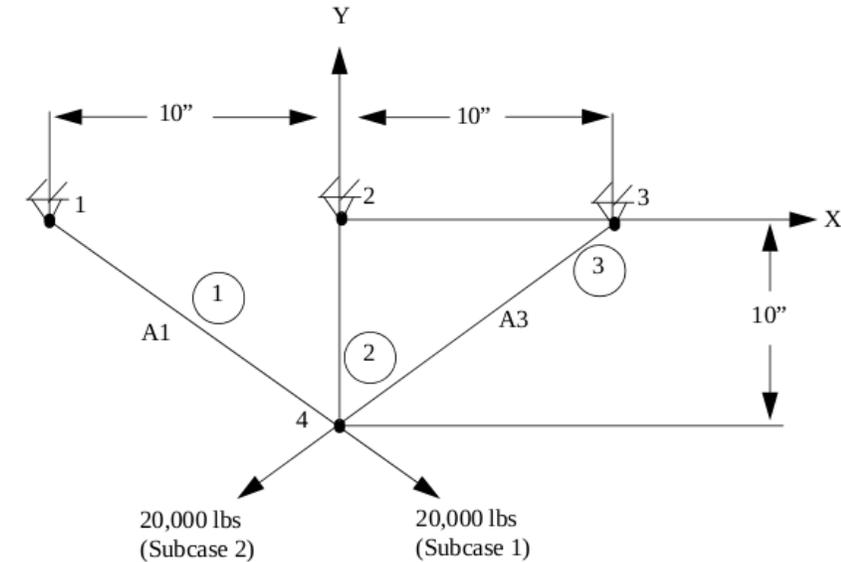


Figure 8-1 Three-Bar Truss

### Analysis Model Description

Three rod (pin-jointed) structure in the x-y plane  
 Symmetric structural configuration with respect to the y axis  
 Two distinct 20,000 lb load conditions

**Material:** E = 1.0E7 psi  
 Weight density = 0.1 lbs/in<sup>3</sup>

### Design Model Description

**Objective:** Minimization of structural weight  
**Design variable:** Cross-sectional areas  $A_1$ ,  $A_2$ , and  $A_3$   
 Design variable linking such that  $A_3 = A_1$   
**Constraints:**  
**Allowable stress:** Tensile 20,000 psi  
 Compressive = -15,000 psi  
**Displacement:**  $\pm 0.2$  at grid 4 in x end of y directions

### Step 0 – Draft the optimization problem statement

- Design Variables – There are 3 design variables
  - x1: Area of element 1
  - x2: Area of element 2
  - x3: Area of element 3
  - The variables are allowed to vary between .001 and 100.
  - The area of element 3 must equal to the area of element 1
    - $x_3 = x_1$
- Design Objective
  - Minimize weight
- Design Constraints
  - g1 - The x and y displacement at node 4 is allowed to be within -.2 and .2 inches
  - g2 - The axial stress in each element is allowed to be within -15000 psi and 20000 psi
  - Both of these constraints are applied to Subcase 1 and 2



### Step 1 - Select an objective

[Switch to Equation Objective](#)

Select an analysis type

SOL 101 - Statics

Select a response

	Response Description	Response Type
	<input type="text"/>	<input type="text"/>
<b>2</b>	Weight	WEIGHT
	Volume	VOLUME
	Displacement	DISP
	Strain	STRAIN
	Element Strain Energy	ESE

« 1 2 3 4 5 »

5 10 20 30 40 50

### Step 2 - Adjust objective

+ Options

	Label	Status	Response Type	Maximize or Minimize	Property Type	ATTA	ATTB	ATTi
	r0		WEIGHT	MIN <b>3</b>		3	3	

## Step 2 – Create Design Objective

1. Navigate to the Objective section
2. Select Weight as the objective from the list of available responses
3. Set the objective to minimize

1

### Step 1 - Select constraints

Select an analysis type

SOL 101 - Statics

Select a response

	Response Description ⇅	Response Type ⇅
	<input type="text" value="s"/>	<input type="text"/>
<input type="checkbox"/>	Displacement	DISP
<input type="checkbox"/>	Strain	STRAIN
<input type="checkbox"/>	Element Strain Energy	ESE
<input type="checkbox"/>	Stress	STRESS
<input type="checkbox"/>	Fatigue, pseudo-static fatigue analysis	FATIGUE

« 1 2 3 4 »

5 10 20 30 40 50

### Step 2 - Adjust constraints

+ Options

	Label ⇅	Status ⇅	Response Type ⇅	Property Type ⇅	ATTA ⇅	ATTB ⇅	ATTi ⇅	Lower Allowed Limit	Upper Allowed Limit
<input type="checkbox"/>									
<input checked="" type="checkbox"/>	r1	<input checked="" type="checkbox"/>	DISP		12 - T1, T2	<input type="text" value="2"/>	4	-2	.2
<input checked="" type="checkbox"/>	r2	<input checked="" type="checkbox"/>	STRESS	PROD	2 - Axial stress	<input type="text" value="2"/>	11, 12, 13	-15000.	20000.

### Step 3 – Create Design Constraints

1. Navigate to the Constraints section
2. Click on the plus icons next to Displacement and Stress to create two constraints
3. Configure the Displacement and Stress constraints

1

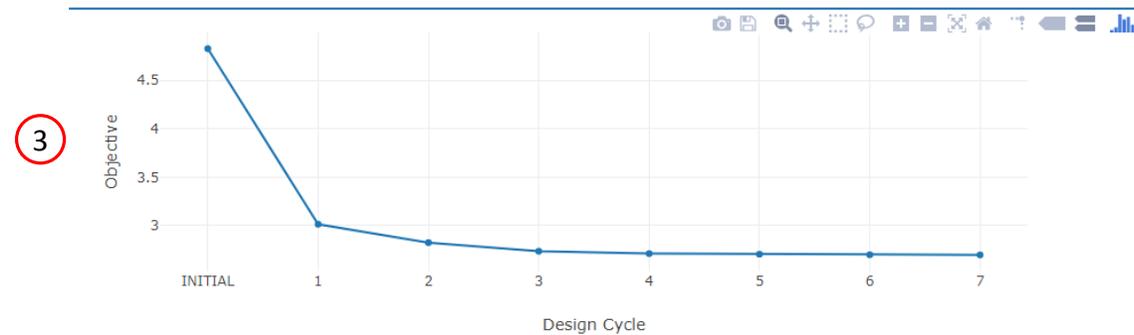
2



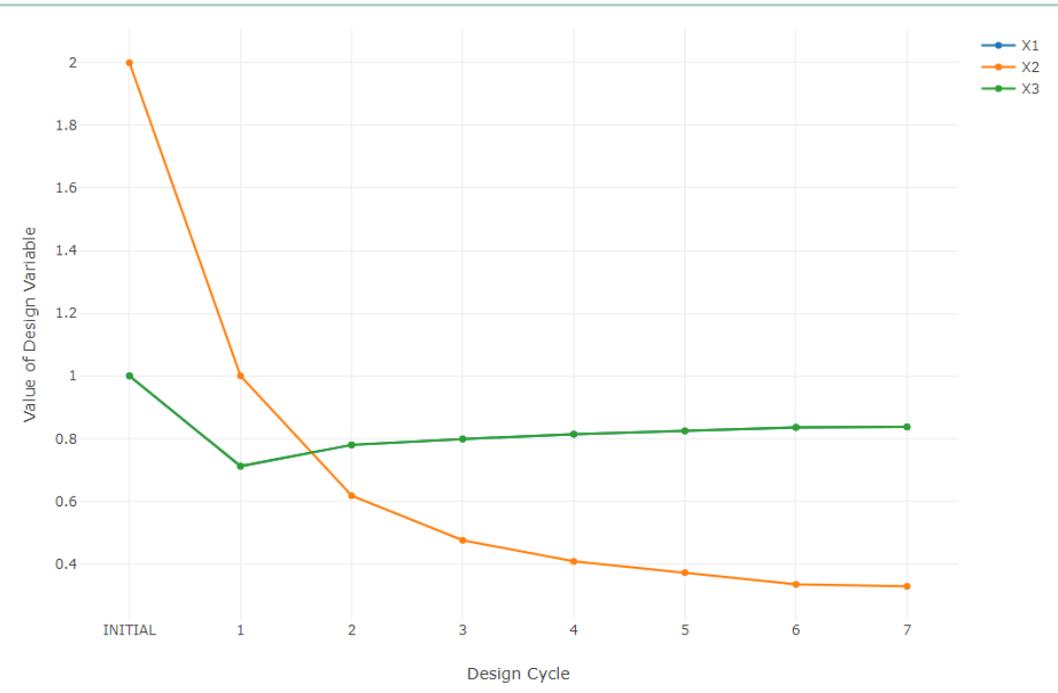
Final Message in .f06

2 ✔ RUN TERMINATED DUE TO HARD CONVERGENCE TO AN OPTIMUM AT CYCLE NUMBER = 7.

Objective

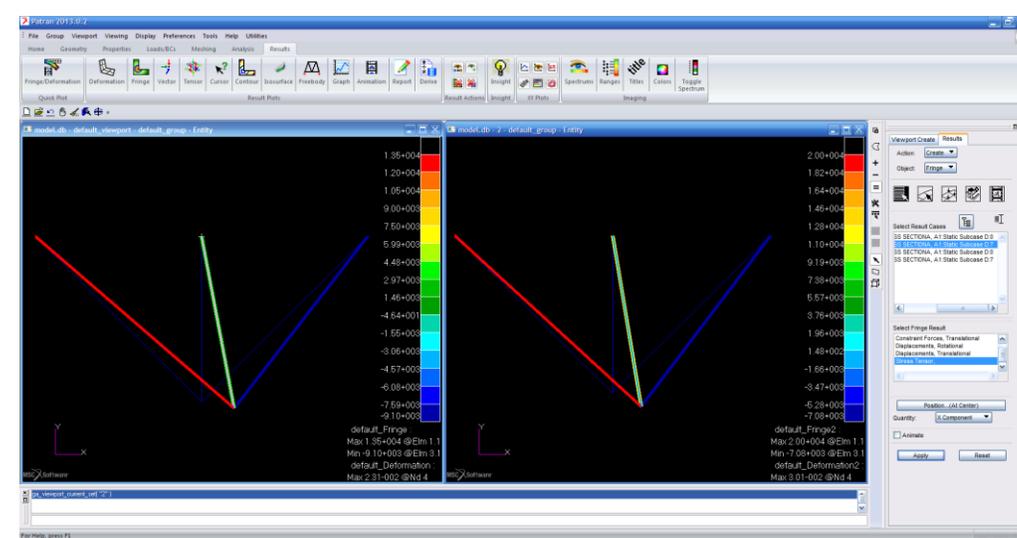


4 Design Variables



Step 5 - Review the results

1. The results are automatically displayed once the optimization is complete
2. The status indicates a successful optimization
3. The change in objective can be viewed
4. The change in design variables can be viewed



A Patran is used to view structural results. Left: Original structural results of the initial design. Right: New structural results of the optimized design.

## Next Steps

- A. The structural results of the optimized design can be viewed in a pre/post processor
- B. The original .bdf file can be updated with new optimized entries found in the .pch file

```

1 $
2 $
3 $
4 $
5 $
6 $
7 $
8 $
9 $
10 $
11 PROD 11 1.83441 0.0 0.0 0.0
12 PROD 12 1.336548 0.0 0.0 0.0
13 PROD 13 1.83441 0.0 0.0 0.0
14

11 ECHO = SORT
12 SPC = 100
13 DISPLACEMENT(SORT1,REAL)=ALL
14 SPOF(SORT1,REAL)=ALL
15 STRESS(SORT1,REAL,VONMISES,BILIN)=ALL
16
17 $ SUBCASE
18 ANALYSIS = STATICS
19 DESOBJ(MEAN) = 8500000
20 DESSUB = $0001
21 SUBCASE 1
22
23 LABEL = LOAD CONDITION 1
24 LOAD = 300
25 SUBCASE 2
26
27 LABEL = LOAD CONDITION 2
28 LOAD = 310
29
30 BEGIN BULK
31 INCLUDE /design_model1.bdf'
32
33 param, post, 1
34
35 $ ANALYSIS MODEL
36 $
37 $
38 $ GRID DATA
39
40 GRID 2 3 4 5 6 7 8 9 10
41
42 GRID 2 -10.0 0.0 0.0
43 GRID 3 0.0 0.0 0.0
44 GRID 4 10.0 0.0 0.0
45 GRID 5 0.0 -10.0 0.0
46
47 $ SUPPORT DATA
48
49 SPC1 100 123456 1 THRU 3
50
51 $ ELEMENT DATA
52
53 CROD 1 11 1 4
54 CROD 2 12 2 4
55 CROD 3 13 3 4
56
57 $ PROPERTY DATA
58
59 PROD 11 1 1.0
60 PROD 12 1 2.0
61 PROD 13 1 1.0
62
63 MAT1 1 1.0E+7 0.33 0.1
64
65 $ FORCE LOAD DATA
66
67 FORCE 300 4 20000. 0.8 -0.6
68 FORCE 310 4 20000. -0.8 -0.6
69
70 ENDDATA
  
```

B Left: The .pch file has the updated PROD entries. Right: The original .bdf file is updated with optimized PROD entries.

# Nastran SOL 200 Learning Resources

Here is a quick summary of helpful tutorials and guides for Nastran SOL 200.

As always, if you have a Nastran SOL 200 question, you are welcome to email me.

Resource	Link
<b>Nastran SOL 200 Tutorials on YouTube</b> Hours of Nastran SOL 200 tutorials are available on my YouTube channel.	<a href="#">Link</a>
<b>Nastran SOL 200 Web App</b> This web application will enable you to convert you existing .bdf files and convert them to SOL 200.	Email me for access
<b>Free Live Training</b> Attend a live training course instructed by me and over 7 hours in length.	<a href="#">Link</a>
<b>Guidance from an Optimization Expert</b> If you are working an optimization project of your own and would like support or guidance, you are welcome to email me.	Email me
<b>MSC Nastran Design Sensitivity and Optimization User's Guide</b> This guide is where I gained a majority of my optimization knowledge and I highly recommend it as a reference.	<a href="#">Link</a>

# Final Comments

You are now one step closer to optimizing structures automatically.

I am here to support you, and if you have any questions regarding Nastran SOL 200, you are welcome to email me.

Thank you for reading this guide and stay motivated.

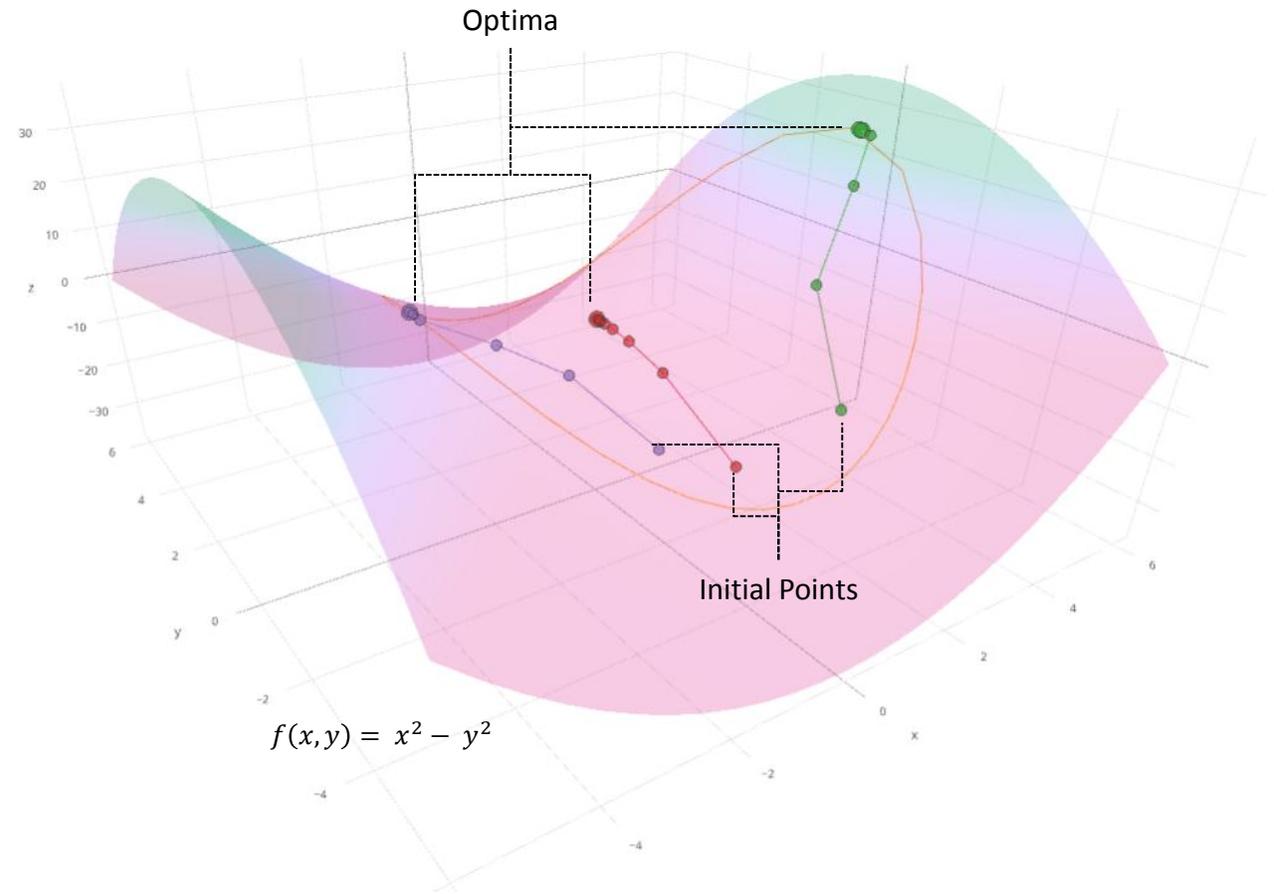
Sincerely,

Christian Aparicio

## One last optimization example

The objective is to find the maximum of  $f(x, y) = x^2 - y^2$  contained within the ellipsoid.  $x$  and  $y$  are allowed to vary. Three optimizations were performed, each represented by the colors purple, red and green. Each optimization had a different initial point. In each scenario, the optimizer

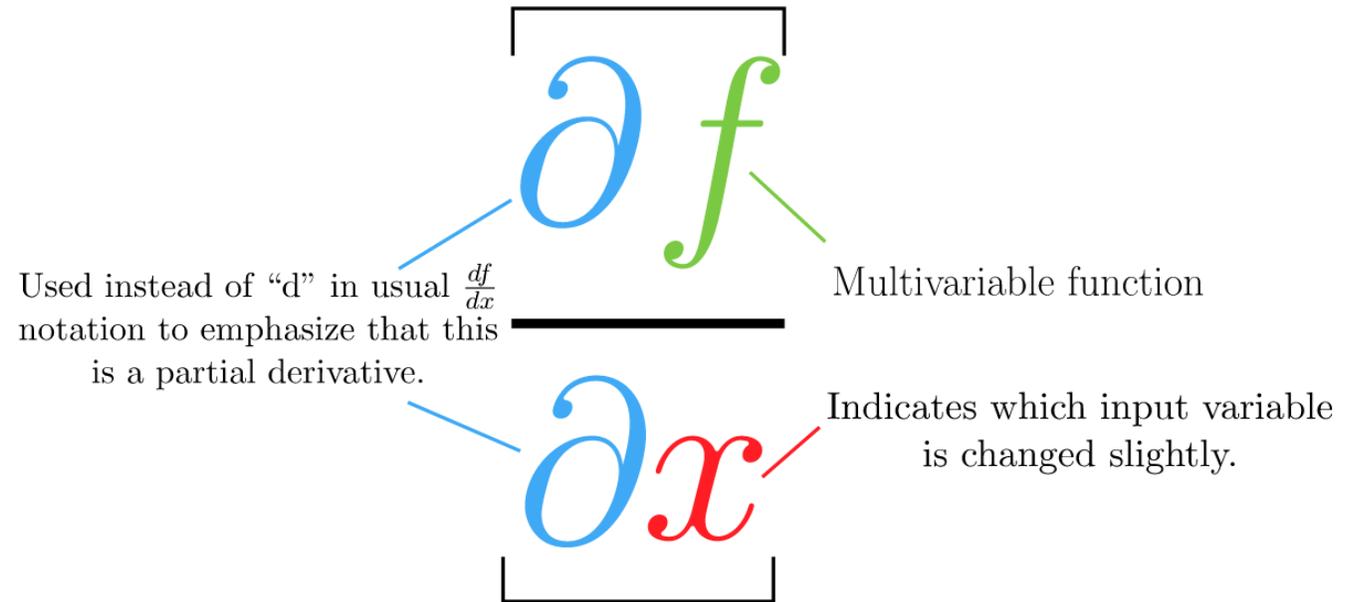
followed the path of steepest ascent (highest gradient), but led to 3 different maxima. When finding optimums of functions with higher dimensions, keep in mind that multiple optimums may exist and that each optimum will depend on your initial design variables.



# Bonus Section – What is Sensitivity Analysis?

---

Can be thought of as “a tiny change in the function’s output”



Can be thought of as “a tiny change in  $x$ ”

Image source: [khanacademy.org – Introduction to Partial Derivatives](https://www.khanacademy.org/introduction-to-partial-derivatives)

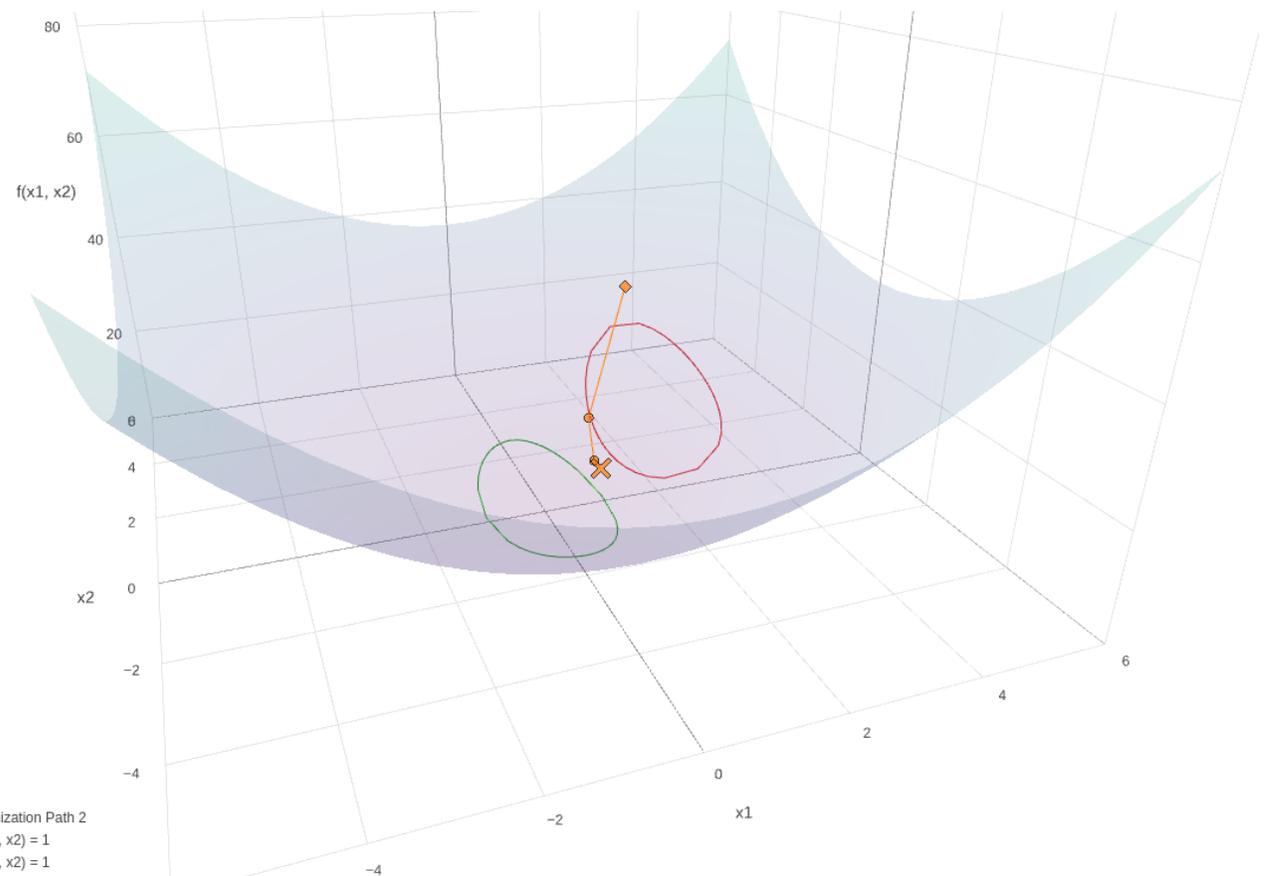
Sensitivity analysis is the process of calculating partial derivatives.

The partial derivatives are commonly referred to as sensitivity coefficients or just sensitivities when using Nastran SOL 200.

Since sensitivities are nothing more than rates of change, design variables can be selected based on their influence on outputs. A question such as this can be answered, which design variable,  $x_1$  or  $x_2$ , if varied, will best minimize the function  $f$ ? Another example, if the goal is to minimize a weight function, it would be logical to select design variables that have sensitivities to the weight.

Let us consider a simple example as shown to the right.

Relevant Equations	Optimization Problem Statement
$f(x_1, x_2) = x_1^2 + x_2^2$	Objective: Minimize $f(x_1, x_2)$
$g_1(x_1, x_2) = x_1^2 + (\frac{x_2}{2})^2$	Initial Point: $(x_1, x_2) = (3, 4)$
$g_2(x_1, x_2) = (x_1 - 2.5)^2 + (\frac{x_2}{2} - .75)^2$	Constraints: $g_1(x_1, x_2) \leq 1$ $g_2(x_1, x_2) \leq 1$



Relevant Equations	Optimization Problem Statement
$f(x_1, x_2) = x_1^2 + x_2^2$ $g_1(x_1, x_2) = x_1^2 + (\frac{x_2}{2})^2$ $g_2(x_1, x_2) = (x_1 - 2.5)^2 + (\frac{x_2}{2} - .75)^2$	Objective: Minimize $f(x_1, x_2)$ Initial Point: $(x_1, x_2) = (3, 4)$ Constraints: $g_1(x_1, x_2) \leq 1$ $g_2(x_1, x_2) \leq 1$

The sensitivities are computed by hand and will be compared to the sensitivities computed by Nastran SOL 200.

$$\frac{\partial f}{\partial x_1} = 2x_1$$

$$\frac{\partial f}{\partial x_1} \Big|_{(3,4)} = 6$$

$$\frac{\partial f}{\partial x_2} = 2x_2$$

$$\frac{\partial f}{\partial x_2} \Big|_{(3,4)} = 8$$

$$\frac{\partial g_1}{\partial x_1} = 2x_1$$

$$\frac{\partial g_1}{\partial x_1} \Big|_{(3,4)} = 6$$

$$\frac{\partial g_1}{\partial x_2} = \frac{x_2}{2}$$

$$\frac{\partial g_1}{\partial x_2} \Big|_{(3,4)} = 2$$

$$\frac{\partial g_2}{\partial x_1} = 2(x_1 - 2.5)$$

$$\frac{\partial g_2}{\partial x_1} \Big|_{(3,4)} = 1$$

$$\frac{\partial g_2}{\partial x_2} = \frac{x_2}{2} - .75$$

$$\frac{\partial g_2}{\partial x_2} \Big|_{(3,4)} = 1.25$$

```

*****
*
*   DESIGN SENSITIVITY MATRIX OUTPUT
*
*   RESPONSE SENSITIVITY COEFFICIENTS
*
*****

```

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0

DRESP2 ID= 9000000		RESPONSE TYPE= SYNTHETIC						SEID= 0	
SUBCASE	RESP VALUE	FREQ/TIME	DESIGN VARIABLE	COEFFICIENT	DESIGN VARIABLE	COEFFICIENT	DESIGN VARIABLE	COEFFICIENT	
0	2.5000E+01	0.0000E+00	4 DUM	0.0000E+00	100001 X1	5.9995E+00	100002 X2	8.0000E+00	

$f(3, 4) = 25$

$\frac{\partial f}{\partial x_1} |_{(3,4)} = 6$

$\frac{\partial f}{\partial x_2} |_{(3,4)} = 8$

DRESP2 ID= 9000001		RESPONSE TYPE= SYNTHETIC						SEID= 0	
SUBCASE	RESP VALUE	FREQ/TIME	DESIGN VARIABLE	COEFFICIENT	DESIGN VARIABLE	COEFFICIENT	DESIGN VARIABLE	COEFFICIENT	
0	1.3000E+01	0.0000E+00	4 DUM	0.0000E+00	100001 X1	6.0000E+00	100002 X2	2.0000E+00	

$g_1(3, 4) = 13$

$\frac{\partial g_1}{\partial x_1} |_{(3,4)} = 6$

$\frac{\partial g_1}{\partial x_2} |_{(3,4)} = 2$

DRESP2 ID= 9000002		RESPONSE TYPE= SYNTHETIC						SEID= 0	
SUBCASE	RESP VALUE	FREQ/TIME	DESIGN VARIABLE	COEFFICIENT	DESIGN VARIABLE	COEFFICIENT	DESIGN VARIABLE	COEFFICIENT	
0	1.8125E+00	0.0000E+00	4 DUM	0.0000E+00	100001 X1	1.0000E+00	100002 X2	1.2500E+00	

$g_2(3, 4) = 1.8125$

$\frac{\partial g_2}{\partial x_1} |_{(3,4)} = 1$

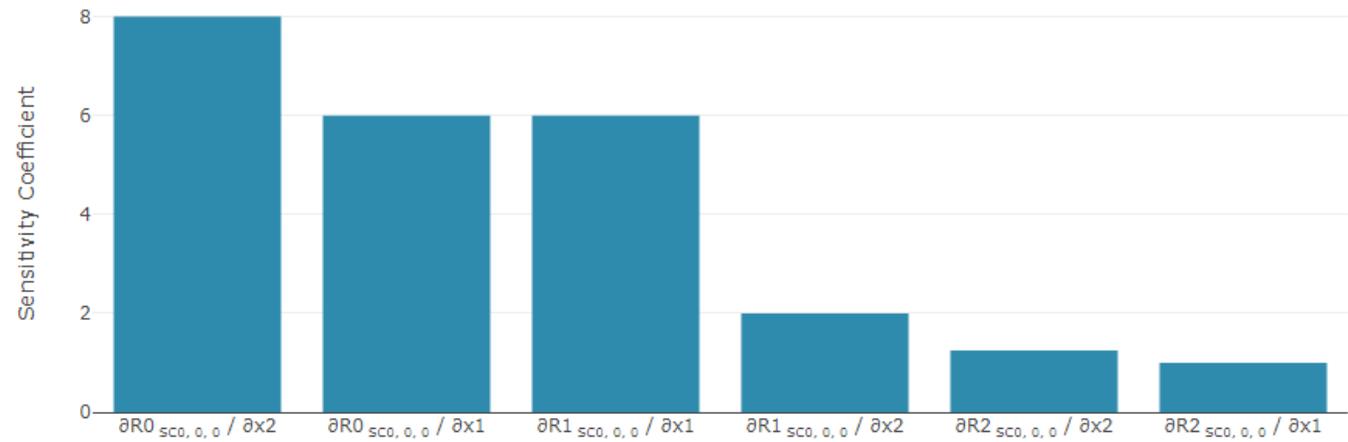
$\frac{\partial g_2}{\partial x_2} |_{(3,4)} = 1.25$

This is the sensitivity output by Nastran SOL 200 and can be found in the .f06 file.

Note that Nastran SOL 200 produces sensitivities in line with the hand calculated sensitivities.

## Sensitivities

Design Sensitivities



The same sensitivities can be automatically plotted in the Nastran SOL 200 Web App

Select a response

Select a design variable

Select a SUBCASE

There are different types of sensitivities you may have to consider.

To the right are some sensitivities and how they are related.

Absolute Sensitivities



Normalized Sensitivities



Normalized Relative Sensitivities

$$\frac{df}{dx_1} = 6$$

$$\begin{aligned}\frac{df}{dx_1} x_1 &= 6 \times 3 \\ &= 18\end{aligned}$$

$$\begin{aligned}\frac{df}{dx_1} \frac{x_1}{f(x_1, x_2)} &= 6 \times \frac{3}{25} \\ &= .72\end{aligned}$$